

An Introduction to Plasma and Feature Scale Modeling in the Semiconductor Industry

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Agenda

- Plasmas in the Semiconductor Industry
- Plasma and Feature Scale Modeling
- Modeling Examples
 - ▶ Global models
 - ▶ Plasma uniformity
 - ▶ Plasma breakdown
 - ▶ Feature scale modeling
 - ▶ Plasma – surface interaction
- Conclusions

Plasmas and the Semiconductor Industry

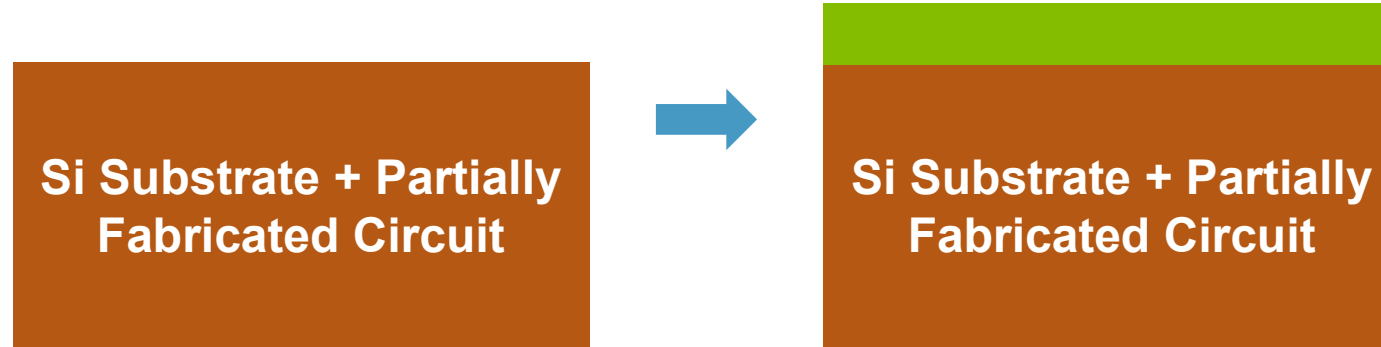
- It's hard to picture life in 2025 without microelectronics—they're everywhere!
- Low-temperature plasmas are a key technology used for microelectronics manufacturing:
 - ▶ Etching
 - ▶ Deposition
 - ▶ Cleaning and surface preparation
 - ▶ Material modification



Plasmas and Microelectronics Fabrication

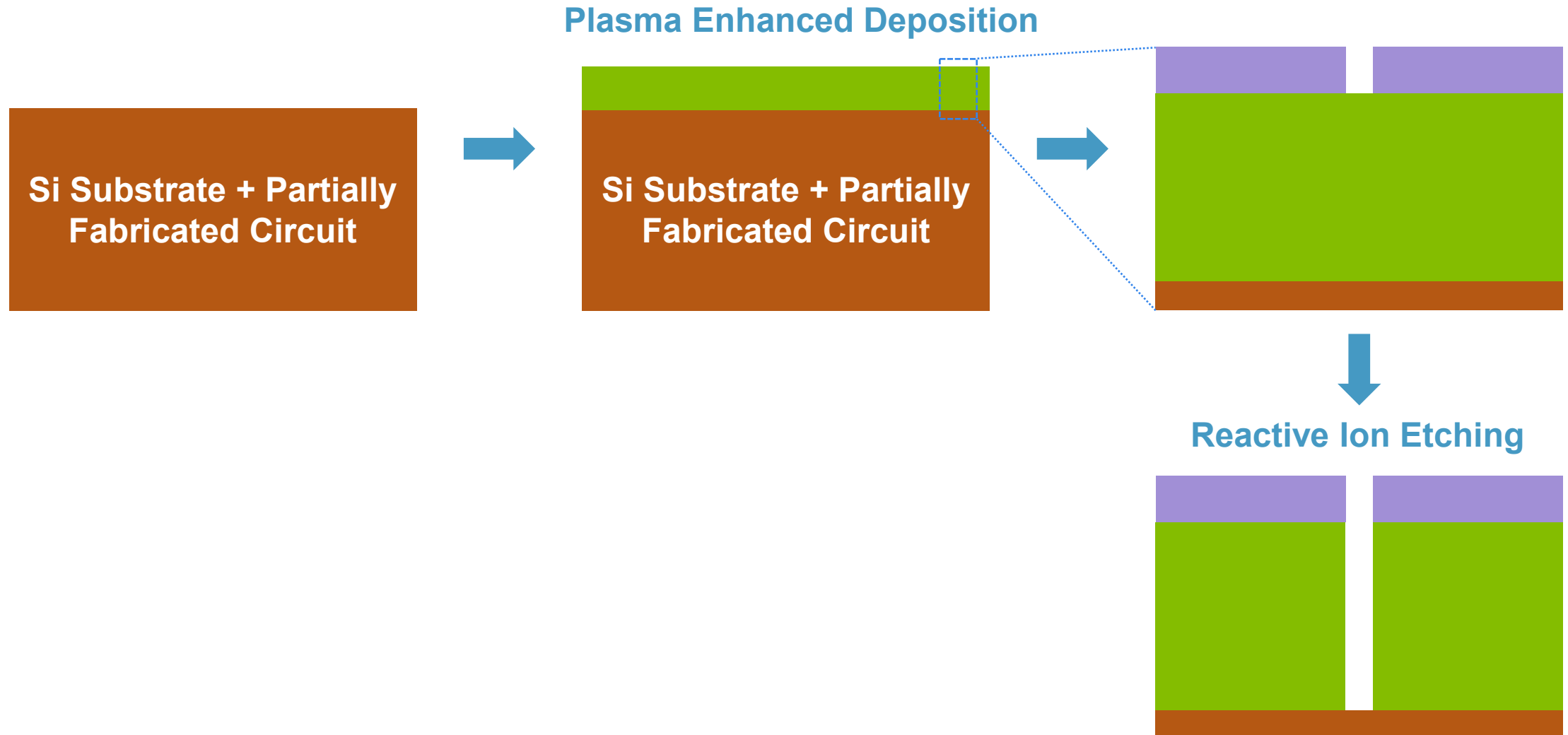
- Microelectronics fabrication requires 100s of processing steps, many plasma based.

Plasma Enhanced Deposition



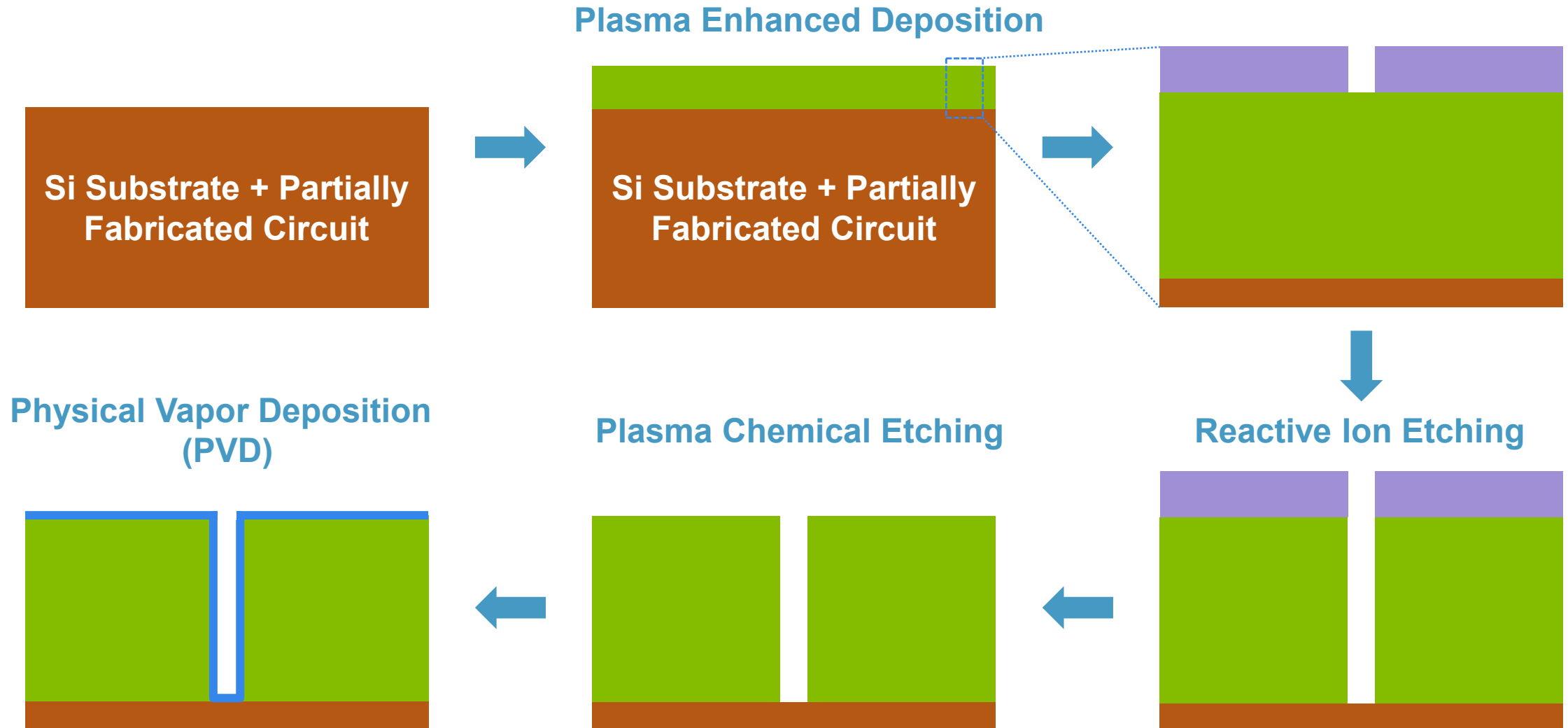
Plasmas and Microelectronics Fabrication

- Microelectronics fabrication requires 100s of processing steps, many plasma based.



Plasmas and Microelectronics Fabrication

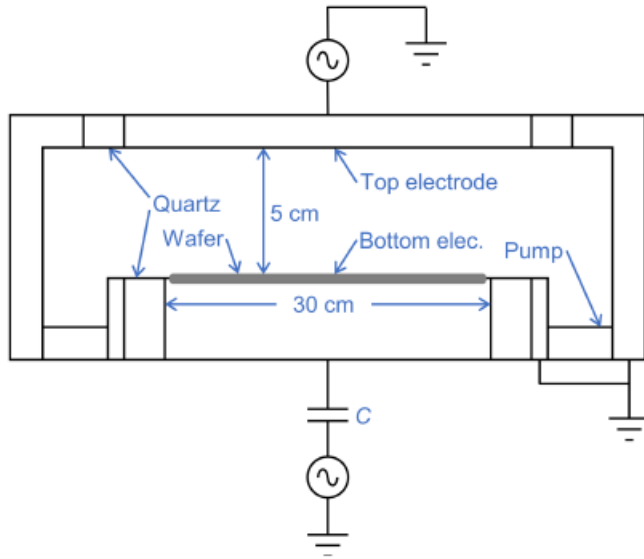
- Microelectronics fabrication requires 100s of processing steps, many plasma based.



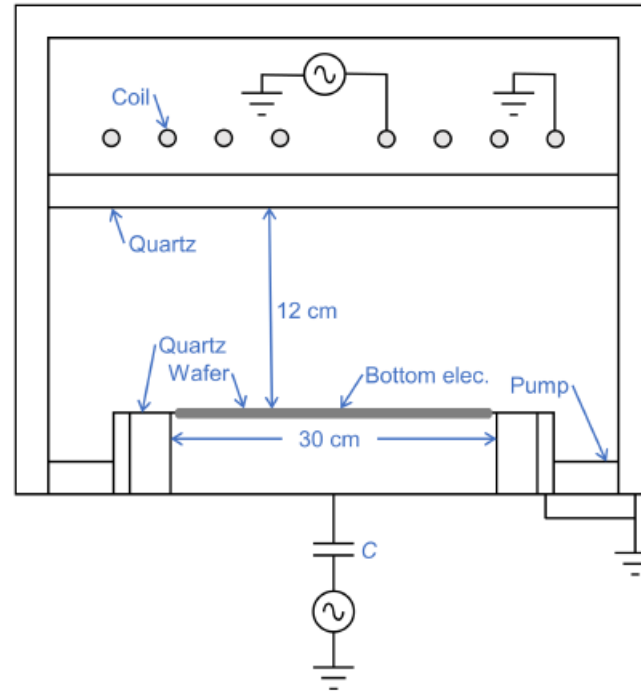
Typical Plasma Sources in Semiconductor Industry

- Many plasma sources are used in the semiconductor industry including the following:

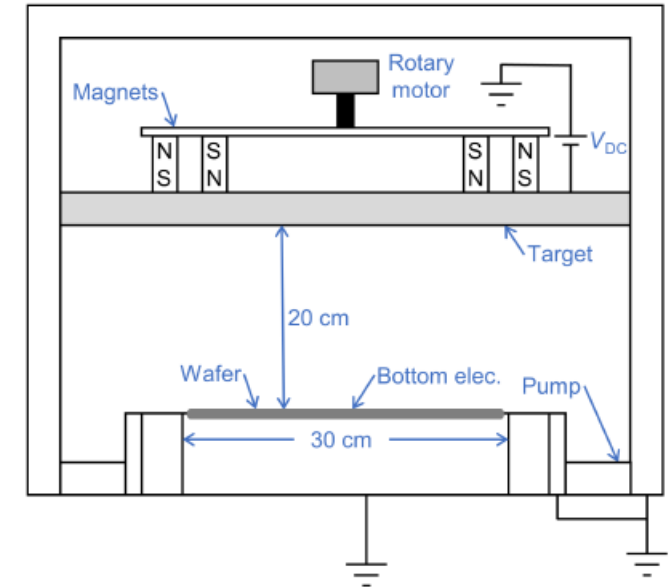
Capacitively Coupled Plasma



Inductively Coupled Plasma



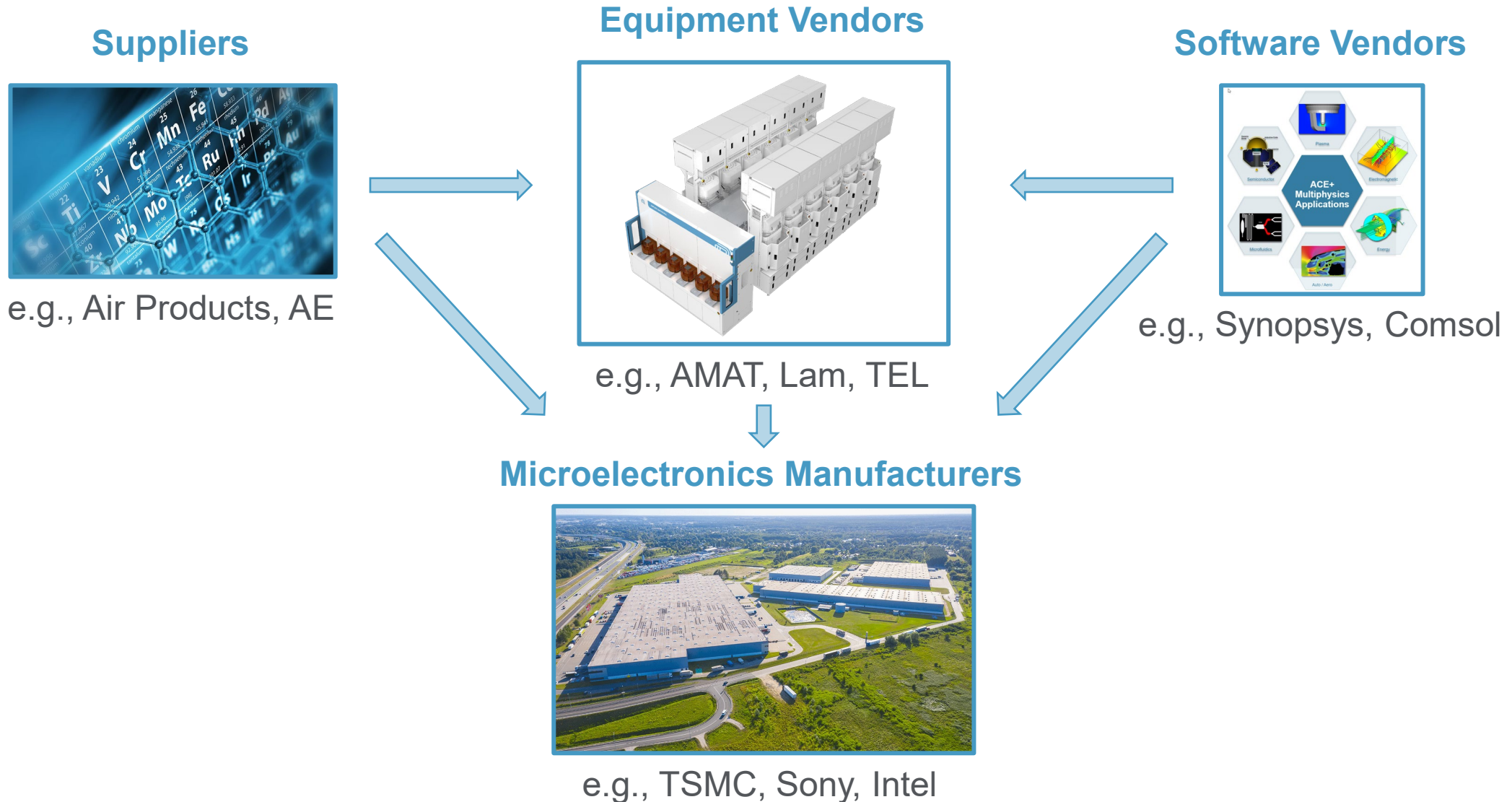
Magnetron Based PVD Source



Plasma and Feature Scale Modeling

Plasma and Feature Scale Modeling Ecosystem in Semiconductor Industry

- Semiconductor industry is one of the largest employers of plasma modeling engineers.



Plasma and Feature Scale Modeling Toolbox

- Plasma modeling engineers in industry:
 - ▶ Actively participate in R&D, product design, and customer communication
 - ▶ Work on a diverse set of technically challenging problems
 - ▶ **Need strong foundation in plasma physics and plasma – surface interactions to be successful**

Plasma and Feature Scale Modeling Toolbox

- Plasma modeling engineers in industry:
 - ▶ Actively participate in R&D, product design, and customer communication
 - ▶ Work on a diverse set of technically challenging problems
 - ▶ **Need strong foundation in plasma physics and plasma – surface interactions to be successful**
 - ▶ Use a variety of specialized software tools

Plasma Modeling

- Global
- Fluid and hybrid
- Kinetic

Feature Scale Modeling

- String and level-set
- Monte Carlo

Atomistic Modeling

- Molecular dynamics
- Quantum chemistry

General Tools

- Python
- Excel
- Fortran / C++

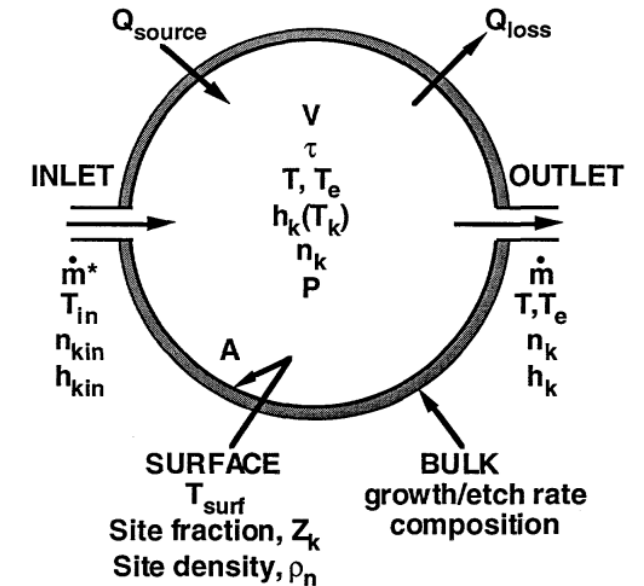
References

Rauf *et al.*, J. Micro/Nanopattern. Mater. Metrol. 22, 041503 (2023)
Kuboi, J. Micro/Nanopattern. Mater. Metrol. 22, 041502 (2023)
Alves *et al.*, Plasma Sources Sci. Technol. 27, 023002 (2018)

Plasma Modeling – Global Models

- Global or 0D models use judicious assumptions to develop simple models for plasma systems:
 - ▶ Spatial shape of plasma, $g_i(\mathbf{x})$
 - ▶ Power deposition mechanism
 - ▶ Electron energy distribution function (EEDF) or Boltzmann equation
- Global models are fast and can afford to model detailed chemistries.
- Plasma physics and chemistry expertise is critical to develop good global models.
- Available global models include:
 - ▶ Quantemol Global Model ([Quantemol-DB](#))
 - ▶ [ZDPlasKin](#)

Well-Stirred Reactor



Lieberman and Lichtenberg, Principles of Plasma Discharges and Materials Processing (2025)
Chabert and Braithwaite, Physics of Radio-Frequency Plasmas (2011)
Meeks *et al.*, AURORA, Sand-96-8218 (1996)

Plasma Modeling – Fluid and Hybrid Models

- Fluid plasma models are the most widely used in industry.
- Fluid models are relatively fast, available in 1, 2, and 3-D, most mature and well-studied, and flexible with many physics options.
- Hybrid models add kinetic treatment of athermal electrons and ions in fluid models.
- Available fluid and hybrid plasma models include:
 - ▶ [Quantemol-VT](#) (HPEM)
 - ▶ CFD-ACE+ ([ACE+ - Applied Materials](#))
 - ▶ [COMSOL Plasma Module](#)
 - ▶ Vizglow ([OverViz - Lam Research](#))

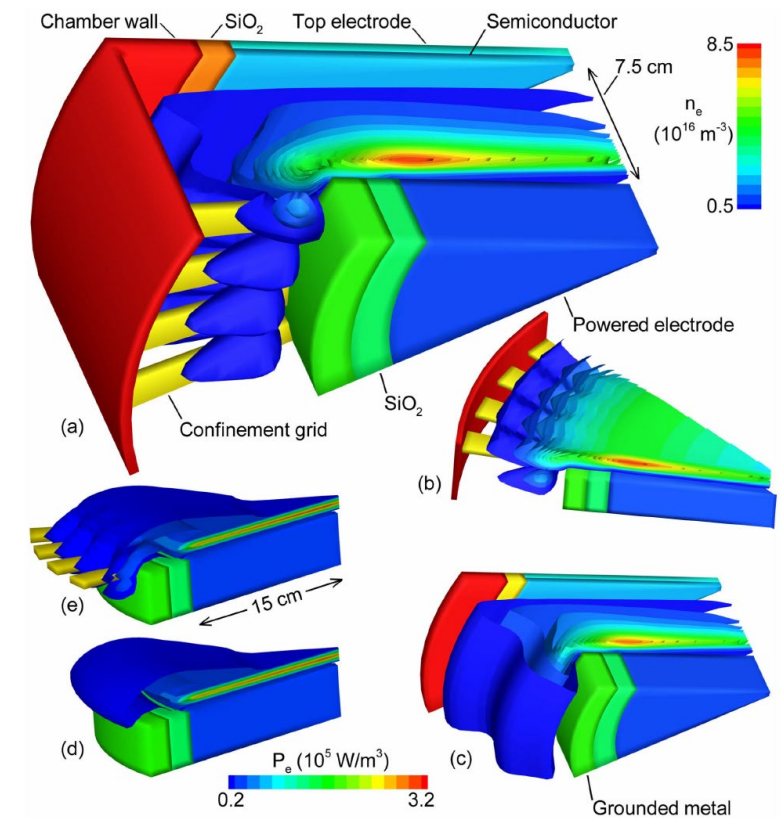


Fig. 1. (a) Electron density in the CCP reactor with the confinement grid, (b) another view of electron density in the reactor with confinement grid, (c) electron density in the system without the confinement grid, (d) electron power deposition without the confinement grid, and (e) electron power deposition in the reactor with confinement grid. Simulations are for 100 mtorr gas pressure in Ar, 500 W applied from bottom electrode at 60 MHz, and 7.5 cm interelectrode spacing. Only a 40° slice is shown for clarity.

Kenney, Rauf, and Collins, IEEE Trans. Plasma Sci. 36, 1364 (2008)

Rauf *et al.*, J. Micro/Nanopattern. Mater. Metrol. 22, 041503 (2023)
Kushner, J. Phys. D: Appl. Phys. 42, 194013 (2009)
Alves *et al.*, Plasma Sources Sci. Technol. 27, 023002 (2018)

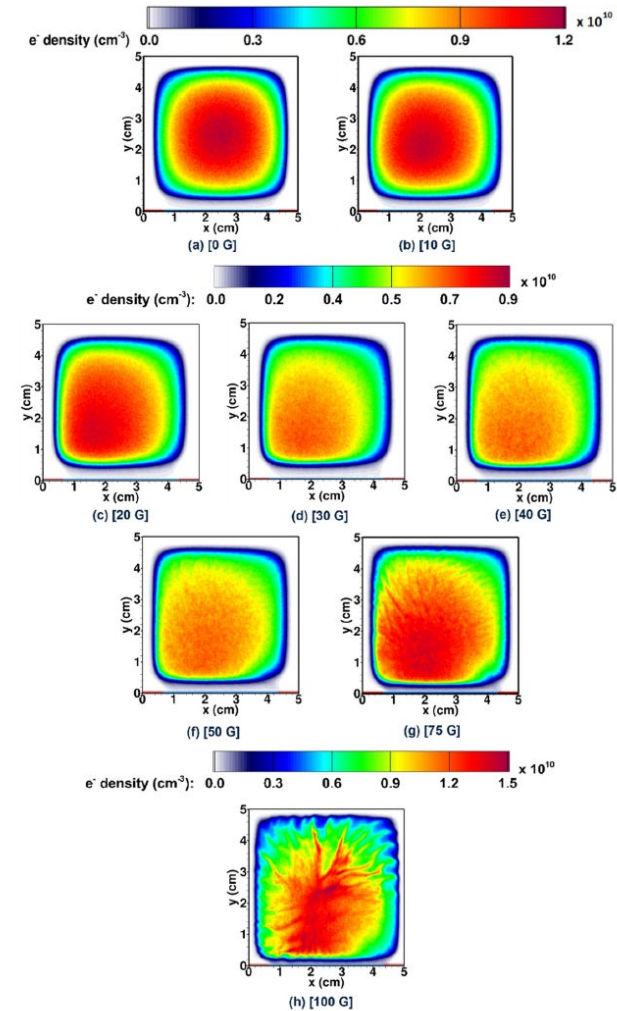
Plasma Modeling – Kinetic Modeling

- Kinetic plasma models become essential for simulating:
 - ▶ low pressure and magnetized plasmas
 - ▶ discharges where kinetic phenomena are important
- Particle-in-Cell with Monte Carlo Collisions (PIC/MCC) is the most widely used kinetic plasma modeling technique.
- PIC simulations are usually slow, and PIC codes are often physics-focused with limited bells-and-whistles for industrial use.
- Available PIC modeling codes include
 - ▶ [EDIPI](#)C (Princeton Plasma Physics Lab)
 - ▶ [WarpX](#) (Lawrence Berkeley Lab)
 - ▶ [VSimPlasma](#) (Tech-X)

References

Birdsall and Langdon, Plasma Physics via Computer Simulation, 1991

Effect of Magnetic Field on Electron Density



Ganta *et al.*, Phys. Plasmas 31, 102107 (2024)

Feature Scale Modeling – Monte Carlo

- Monte Carlo methods are commonly used to model plasma interaction with surfaces.
- These models approximate the material as a 2 or 3-D array of voxels representing atomic clusters.
- Plasma species with given fluxes and energy + angular distributions are introduced from the top.
- The reaction mechanism dictates the interaction of ions and neutrals from the plasma with the surface.
- Available Monte Carlo feature scale model include:
 - MCFPM (University of Michigan)
 - Pagasus [FPSM2D](#)

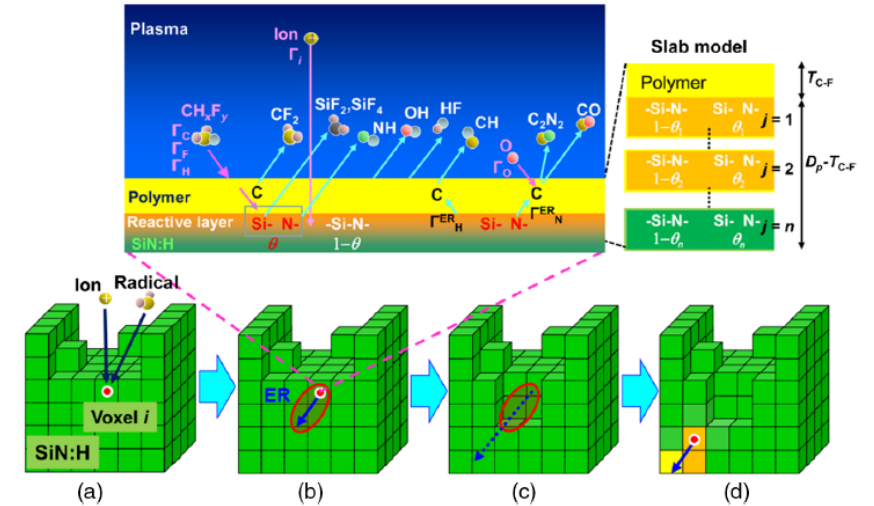


Fig. 19 Schematic drawing of calculation procedure through (a), (b), (c), and (d) for 3D voxel-slab model.⁶⁹

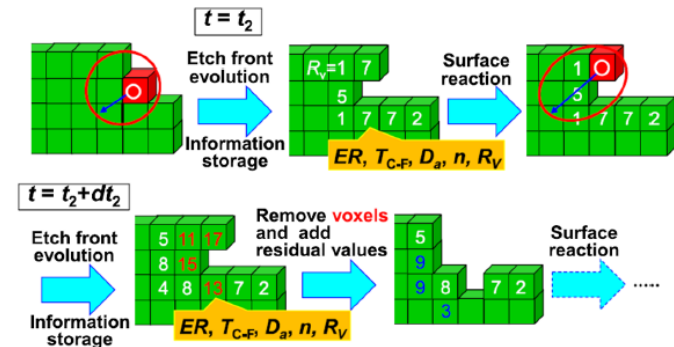
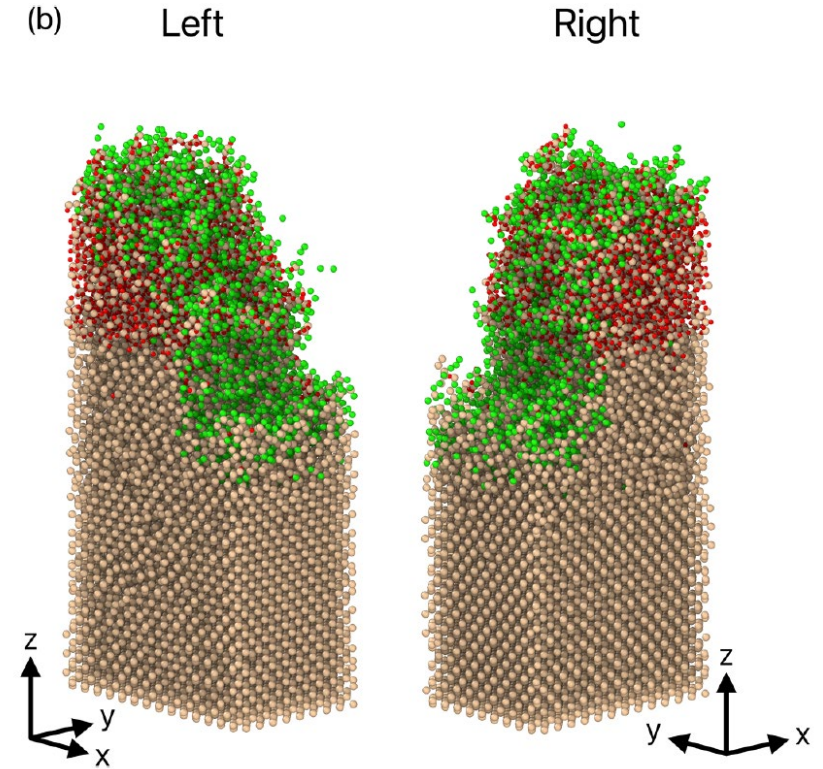


Fig. 20 Schematic drawing of etch front evolution for 3D voxel-slab model. The red circle at the red voxel represents an etched region related to the derive ER and red values in voxels exceed the threshold to be removed.⁶⁹

Atomistic Modeling – Molecular Dynamics

- Molecular dynamics (MD) is a widely used technique in material science and quantum chemistry.
- MD combines potentials (derived from ab-initio computations) with classical physics to simulate the dynamics of large cluster of atoms.
- MD is used by the low-temperature plasma community to study plasma etch processes.
- Availability and accuracy of potentials are important issues in MD modeling.
- Many MD models are available ([MD Software – Wikipedia](#)) including:
 - ▶ [LAMMPS](#) (Sandia National Lab)

MD Simulation of SiO₂/Si Etch



Mauchamp and Hamaguchi, J. Vac. Sci. Technol. A 40, 053004 (2022)

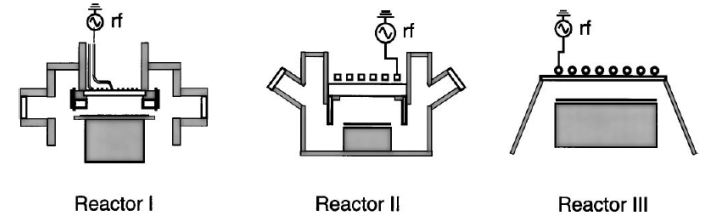
Frenkel and Smit, Understanding Molecular Simulation (2001)
Griebel, Knapek, and Zumbusch, Numerical Simulation in Molecular Dynamics (2010)
Mubin and Li, Extending and Modifying LAMMPS (2021)

Modeling Examples

Ho – SiO₂ Etch in C₂F₆ Plasma – Model

- Ho *et al.* developed a 0D model for SiO₂ etch in C₂F₆ plasma using Aurora.
- C₂F₆ mechanism: 28 species and 132 reactions.
- SiO₂ etch mechanism: 6 species and 85 reactions.
- Assumptions: spatially uniform, Maxwellian electrons.
- Tested the model using experimental data from 3 ICP reactors.

ICP Reactors



Mechanism – C₂F₆ Plasma and SiO₂ Etch

TABLE I. Gas-phase reaction mechanism for C₂F₆ plasma etching of silicon dioxide^a

Reaction No.	Reaction	A	B	C	e	Notes	Reference
(1)	$e + C_2F_6 \rightarrow CF_2 + e$	2.12E-7	0.3252	3.67E3	0.14	V ^{0.5}	42
(2)	$e + C_2F_6 \rightarrow CF_2 + e$	6.78E-8	0.4238	8.17E3	0.14	V ^{0.5}	42
(3)	$e + C_2F_6 \rightarrow CF_2 + e$	3.79E-4	0.7779	2.19E4	0.15	V ^{0.5}	42
(4)	$e + C_2F_6 \rightarrow CF_2 + e$	3.83E-3	1.142	1.15E5	0.2	V ^{0.5}	42
(5)	$e + C_2F_6 \rightarrow CF_2 + e$	1.89E-12	0.6066	1.14E3	0.11	V ^{0.5}	42
(6)	$e + C_2F_6 \rightarrow CF_2 + e$	3.12E-8	0.1003	1.59E5	0.13	V ^{0.5}	42
(7)	$e + C_2F_6 \rightarrow CF_2 + e$	2.48E-12	0.8790	1.67E3	0.15	V ^{0.5}	42
(8)	$e + C_2F_6 \rightarrow CF_2 + e$	3.29E-13	0.8655	2.40E5	0.17	V ^{0.5}	42
(9)	$e + C_2F_6 \rightarrow CF_2 + e$	7.89E-14	1.809	1.97E5	0.18	V ^{0.5}	42
(10)	$e + C_2F_6 \rightarrow CF_2 + e$	2.51E-7	0.6387	4.61E4	0.25	V ^{0.5}	42
(11)	$e + C_2F_6 \rightarrow CF_2 + e$	6.42E-7	0.3188	3.99E5	0.11	V ^{0.5}	44
(12)	$e + C_2F_6 \rightarrow CF_2 + e$	9.94E-9	0.2802	1.56E5	0.05	V ^{0.5}	44
(13)	$e + C_2F_6 \rightarrow CF_2 + e$	0.2	1.367	7.74E4	0.4	V ^{0.5}	44
(14)	$e + C_2F_6 \rightarrow CF_2 + e$	1.19E-16	1.309	1.44E5	0.6	V ^{0.5}	44
(15)	$e + C_2F_6 \rightarrow CF_2 + e$	7.73E-17	1.184	1.60E5	0.5	V ^{0.5}	44
(16)	$e + C_2F_6 \rightarrow CF_2 + e$	1.03E-16	1.187	2.20E5	0.49	V ^{0.5}	44
(17)	$e + C_2F_6 \rightarrow CF_2 + e$	1.15E-11	0.7545	1.93E5	0.15	V ^{0.5}	44
(18)	$e + C_2F_6 \rightarrow CF_2 + e$	2.84E-11	0.5108	2.44E5	0.22	V ^{0.5}	44
(19)	$e + C_2F_6 \rightarrow CF_2 + e$	2.24E-14	1.809	3.13E5	0.7	V ^{0.5}	44
(20)	$e + C_2F_6 \rightarrow CF_2 + e$	1.48E-13	0.8375	4.82E5	0.21	V ^{0.5}	44
(21)	$e + C_2F_6 \rightarrow CF_2 + e$	3.61E-17	1.413	3.94E5	0.36	V ^{0.5}	44
(22)	$e + C_2F_6 \rightarrow CF_2 + e$	1.89E-12	2.411	3.91E5	0.4	V ^{0.5}	44
(23)	$e + C_2F_6 \rightarrow CF_2 + e$	4.48E-10	3.880	3.51E5	0.2	V ^{0.5}	44
(24)	$e + C_2F_6 \rightarrow CF_2 + e$	2.34E-8	0.4895	5.87E4	0.3	V ^{0.5}	44
(25)	$e + C_2F_6 \rightarrow CF_2 + e$	4.63E-4	0.8407	1.50E5	0.3	V ^{0.5}	44
(26)	$e + C_2F_6 \rightarrow CF_2 + e$	1.4E-11	0.6481	1.13E5	0.1	V ^{0.5}	44
(27)	$e + C_2F_6 \rightarrow CF_2 + e$	1.37E-10	0.6467	1.90E5	0.17	V ^{0.5}	44
(28)	$e + C_2F_6 \rightarrow CF_2 + e$	5.05E-11	0.5960	2.45E5	0.24	V ^{0.5}	44
(29)	$e + C_2F_6 \rightarrow CF_2 + e$	5.58E-10	0.2996	3.34E5	0.21	V ^{0.5}	44
(30)	$e + C_2F_6 \rightarrow CF_2 + e$	2.34E-8	0.4895	5.87E4	0.4	V ^{0.5}	44
(31)	$e + C_2F_6 \rightarrow CF_2 + e$	3.43E-4	0.8406	9.01E4	0.6	V ^{0.5}	44
(32)	$e + C_2F_6 \rightarrow CF_2 + e$	1.79E-4	0.818	4.75E4	0.2	V ^{0.5}	44
(33)	$e + C_2F_6 \rightarrow CF_2 + e$	1.19E-16	1.309	1.44E5	0.4	V ^{0.5}	44
(34)	$e + C_2F_6 \rightarrow CF_2 + e$	1.57E-11	0.6287	1.23E5	0.16	V ^{0.5}	44
(35)	$e + C_2F_6 \rightarrow CF_2 + e$	2.45E-12	0.7063	1.60E5	0.12	V ^{0.5}	44
(36)	$e + C_2F_6 \rightarrow CF_2 + e$	1.67E-9	0.2119	4.44E5	0.22	V ^{0.5}	44
(37)	$e + C_2F_6 \rightarrow CF_2 + e$	3.40E-8	0.4895	5.87E4	0.9	V ^{0.5}	44
(38)	$e + C_2F_6 \rightarrow CF_2 + e$	1.19E-16	1.309	1.44E5	0.6	V ^{0.5}	44
(39)	$e + C_2F_6 \rightarrow CF_2 + e$	1.27E-15	1.028	1.67E5	0.11	V ^{0.5}	44
(40)	$e + C_2F_6 \rightarrow CF_2 + e$	2.30E-7	0.4893	5.87E4	0.21	V ^{0.5}	44
(41)	$e + C_2F_6 \rightarrow CF_2 + e$	4.83E-6	0.5042	2.49E4	1.264	Z ^{1.7}	48
(42)	$e + C_2F_6 \rightarrow CF_2 + e$	6.89E-7	0.5041	4.10E4	0.84	Z ^{1.7}	48
(43)	$e + C_2F_6 \rightarrow CF_2 + e$	1.58E-6	0.6704	1.66E5	1.27	E ^{3.4}	48
(44)	$e + C_2F_6 \rightarrow CF_2 + e$	5.95E-9	0.0238	1.60E5	12.983	E ^{3.4}	48
(45)	$e + C_2F_6 \rightarrow CF_2 + e$	7.48E-13	0.8795	2.62E5	17.42	V ^{0.5}	48
(46)	$e + C_2F_6 \rightarrow CF_2 + e$	4.78E-3	1.371	4.74E5	0.02	V ^{0.5}	48
(47)	$e + C_2F_6 \rightarrow CF_2 + e$	4.78E-3	1.371	4.74E5	0.02	V ^{0.5}	48
(48)	$e + C_2F_6 \rightarrow CF_2 + e$	2.94E-6	0.4119	4.69E5	0.10	V ^{0.5}	48
(49)	$e + C_2F_6 \rightarrow CF_2 + e$	2.54E-12	0.8182	1.80E5	0.22	V ^{0.5}	48
(50)	$e + C_2F_6 \rightarrow CF_2 + e$	1.22E-8	0.0134	1.88E5	11.9	V ^{0.5}	48
(51)	$e + C_2F_6 \rightarrow CF_2 + e$	1.03E-16	1.187	2.20E5	0.49	V ^{0.5}	48
(52)	$e + C_2F_6 \rightarrow CF_2 + e$	2.50E-11	0.6641	2.02E5	0.6	V ^{0.5}	48
(53)	$e + C_2F_6 \rightarrow CF_2 + e$	2.88E-11	0.5108	2.44E5	0.22	V ^{0.5}	48
(54)	$e + C_2F_6 \rightarrow CF_2 + e$	2.24E-14	1.809	3.13E5	0.7	V ^{0.5}	48
(55)	$e + C_2F_6 \rightarrow CF_2 + e$	1.48E-13	0.8375	4.82E5	0.21	V ^{0.5}	48
(56)	$e + C_2F_6 \rightarrow CF_2 + e$	1.24E-8	0.3792	1.14E5	0.3	V ^{0.5}	48
(57)	$e + C_2F_6 \rightarrow CF_2 + e$	1.19E-16	1.309	1.44E5	0.6	V ^{0.5}	48
(58)	$e + C_2F_6 \rightarrow CF_2 + e$	1.03E-16	1.187	2.20E5	0.49	V ^{0.5}	48
(59)	$e + C_2F_6 \rightarrow CF_2 + e$	2.34E-8	0.4895	5.87E4	0.4	V ^{0.5}	48
(60)	$e + C_2F_6 \rightarrow CF_2 + e$	1.99E-10	0.4660	1.73E5	15.90	V ^{0.5}	48
(61)	$e + C_2F_6 \rightarrow CF_2 + e$	7.04E-12	0.6944	1.974E5	17.43	V ^{0.5}	48

TABLE II. (Continued)

Reaction No.	Reaction	A	B	C	e	Notes	Reference
(62)	$e + SiF_4 \rightarrow SiF_2 + e$	1.80E-10	0.3139	3.34E5	0.25	V ^{0.5}	53
(63)	$e + SiF_4 \rightarrow SiF_2 + e$	1.54E-8	0.3792	1.14E5	0.0	V ^{0.5}	53
(64)	$e + SiF_4 \rightarrow SiF_2 + e$	1.19E-16	1.309	1.44E5	0.6	V ^{0.5}	53
(65)	$e + SiF_4 \rightarrow SiF_2 + e$	2.62E-9	0.2550	1.44E5	10.80	V ^{0.5}	53
(66)	$e + SiF_4 \rightarrow SiF_2 + e$	3.57E-13	0.9855	1.59E5	0.12	V ^{0.5}	54
(67)	$e + SiF_4 \rightarrow SiF_2 + e$	7.94E-11	0.4722	3.49E5	0.24	V ^{0.5}	54
(68)	$e + SiF_4 \rightarrow SiF_2 + e$	1.24E-8	0.3792	1.14E5	0.0	V ^{0.5}	54
(69)	$e + SiF_4 \rightarrow SiF_2 + e$	1.19E-16	1.309	1.44E5	0.6	V ^{0.5}	54
(70)	$e + SiF_4 \rightarrow SiF_2 + e$	2.62E-9	0.2550	1.44E5	10.80	V ^{0.5}	54
(71)	$e + SiF_4 \rightarrow SiF_2 + e$	3.88E-10	0.4391	1.62E5	14.3	V ^{0.5}	55
(72)	$e + SiF_4 \rightarrow SiF_2 + e$	7.11E-11	0.3862	2.38E5	23.1	V ^{0.5}	55
(73)	$e + SiF_4 \rightarrow SiF_2 + e$	1.24E-8	0.379	1.14E5	0.0	V ^{0.5}	55
(74)	$e + SiF_4 \rightarrow SiF_2 + e$	3.10E-7	0.987	2.21E4	0.19	V ^{0.5}	55
(75)	$e + SiF_4 \rightarrow SiF_2 + e$	3.00E-4	1.02	5.33E4	0.08	V ^{0.5}	55
(76)	$e + SiF_4 \rightarrow SiF_2 + e$	4.79E-5	0.9297	5.63E4	0.38	V ^{0.5}	55
(77)	$e + SiF_4 \rightarrow SiF_2 + e$	2.87E-4	1.133	5.65E4	0.57	V ^{0.5}	55
(78)	$e + SiF_4 \rightarrow SiF_2 + e$	1.88E-3	1.338	5.63E4	0.75	V ^{0.5}	55
(79)	$e + SiF_4 \rightarrow SiF_2 + e$	1.42E-6	0.5966	5.73E4	0.98	V ^{0.5}	55
(80)	$e + SiF_4 \rightarrow SiF_2 + e$	3.02E-7	0.739	6.21E4	1.43	V ^{0.5}	55
(81)	$e + SiF_4 \rightarrow SiF_2 + e$	2.28E-10	0.4019	6.80E4	4.2	V ^{0.5}	56
(82)	$e + SiF_4 \rightarrow SiF_2 + e$	1.88E-4	1.267	5.44E4	0.4	V ^{0.5}	56
(83)	$e + SiF_4 \rightarrow SiF_2 + e$	4.82E-4	0.4483	5.71E4	4.0	V ^{0.5}	56
(84)	$e + SiF_4 \rightarrow SiF_2 + e$	4.24E-10	0.3654	5.61E4	8.4	V ^{0.5}	56
(85)	$e + SiF_4 \rightarrow SiF_2 + e$	1.37E-18	1.29	7.57E4	10.0	V ^{0.5}	56
(86)	$e + SiF_4 \rightarrow SiF_2 + e$	8.40E-16	1.121	7.57E4	14.7	V ^{0.5}	56
(87)	$e + SiF_4 \rightarrow SiF_2 + e$	1.64E-15	1.419	6.49E4	12.1	V ^{0.5}	56
(88)	$e + SiF_4 \rightarrow SiF_2 + e$	9.60E-7	0.4471	5.50E4	1.97	V ^{0.5}	56
(89)	$e + SiF_4 \rightarrow SiF_2 + e$	2.75E-8	0.3588	6.25E4	1.9	V ^{0.5}	56
(90)	$e + SiF_4 \rightarrow SiF_2 + e$	2.54E-15	1.328	6.05E4	16.4	V ^{0.5}	56
(91)	$e + SiF_4 \rightarrow SiF_2 + e$	0.00164	1.434	2.23E4	0.27	V ^{0.5}	60
(92)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01313	1.413	2.14E4	0.33	V ^{0.5}	60
(93)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(94)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(95)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(96)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(97)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(98)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(99)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(100)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(101)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(102)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(103)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(104)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(105)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(106)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(107)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(108)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(109)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(110)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(111)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(112)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(113)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(114)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(115)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(116)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(117)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(118)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(119)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60
(120)	$e + SiF_4 \rightarrow SiF_2 + e$	0.01319	1.421	2.07E4	0.79	V ^{0.5}	60

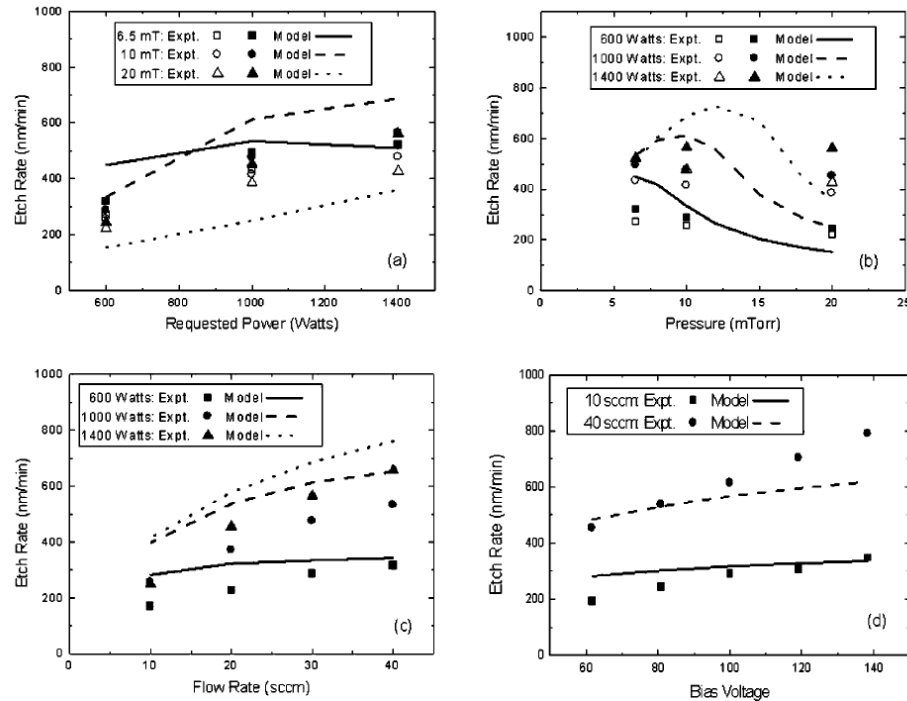
TABLE III. (Continued)

Reaction No.	Reaction	A	B	C	e	Notes	Referen
(121)	$F + O_2 \rightarrow O_2 + F$ low- α_2 perturbation	$7.007E-10$	0.0	0.0	0.0		63
(122)	$F + CF_2 \rightarrow 2F + CF_2$	$4.0E-7$	-0.5	0.0		Estimate	
(123)	$F + CF_2 \rightarrow F + CF_2$	$4.0E-7$	-0.5	0.0		Estimate	
(124)	$F + CF_2 \rightarrow 2F + C$	$4.0E-7$	-0.5	0.0		Estimate	
(125)	$F + F^+ \rightarrow 2F^+$	$4.0E-7$	-0.5	0.0		Estimate	
(126)	$F + SF_2 \rightarrow F + S$	$4.0E-7$	-0.5	0.0		Estimate	
(127)	$F + SF_2^+ \rightarrow F + SF_2^+$	$4.0E-7$	-0.5	0.0		Estimate	
(128)	$F + SF_2^+ \rightarrow F + SF_2^+$	$4.0E-7$	-0.5	0.0		Estimate	
(129)	$F + SF_2^+ \rightarrow SF_2 + SF_2^+$	$4.0E-7$	-0.5	0.0		Estimate	
(130)	$F + O^+ \rightarrow F + O$	$4.0E-7$	-0.5	0.0		Estimate	
(131)	$F + CO \rightarrow F + CO$	$4.0E-7$	-0.5	0.0		Estimate	
(132)	$F + CO^+ \rightarrow F + CO$	$4.0E-7$	-0.5	0.0		Estimate	

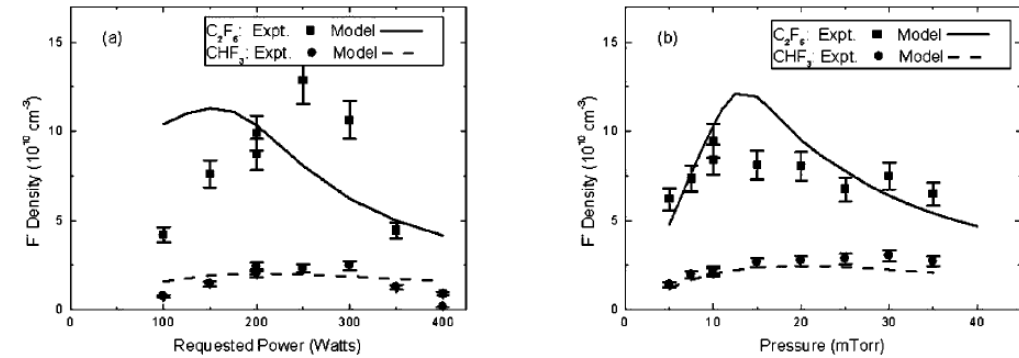
Ho – SiO₂ Etch in C₂F₆ Plasma – Comparison to Experiments

- Ho *et al.* compared their 0D modeling results to a wide variety of experimental data:
 - SiO₂ etch rate over a range of conditions in 2 chambers
 - F, SiF, and CF_x radical densities
 - Electron density

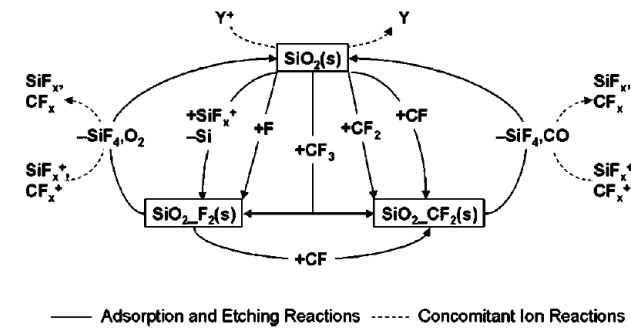
Etch Rate – Model vs. Experiment



F Density – Model vs. Experiment



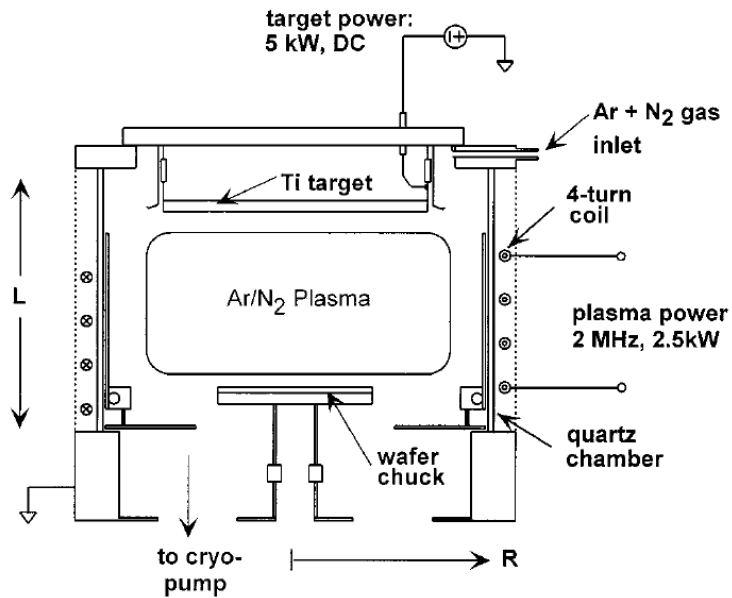
SiO₂ Etch Mechanism – Reactor III



Tao – Ionized PVD of TiN – Model

- Tao, Mao, and Hopwood developed a global model for TiN ionized physical vapor deposition (IPVD).
- Model targeted towards 1 experimental system.
- Plasma chemistry is relatively simple with important Ar, N and Ti species included.
- Assumptions: volume averaged densities, sputtered Ti fully thermalized, TiN forms on surface.

TiN IPVD Reactor



Ti/Ar/N₂ Plasma Chemistry

Reaction	Rate constants	Reference
$N + e^- \rightarrow N^+ + 2e^-$	$K_1 = 3.84 \times 10^{-9} (T_e)^{0.92} \exp(-12.1/T_e) \text{ cm}^3 \text{ s}^{-1}$	a
$N_2 + e^- \rightarrow N_2^+ + 2e^-$	$K_2 = 1.95 \times 10^{-9} (T_e)^{1.13} \exp(-14.4/T_e) \text{ cm}^3 \text{ s}^{-1}$	b
$N_2 + e^- \rightarrow 2N + e^-$	$K_3 = 6.15 \times 10^{-9} (T_e)^{0.81} \exp(-12.8/T_e) \text{ cm}^3 \text{ s}^{-1}$	c
$N^+ + N_2 \rightarrow N_2^+ + N$	$K_5 = 2.0 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$	d
$N + N_2^+ \rightarrow N^+ + N_2$	$K_6 = 1.0 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$	e
$N_2^* + N \rightarrow N + N_2$	$K_7 = 4.0 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$	f
$N_2^* + N_2 \rightarrow 2N_2$	$K_8 = 3.5 \times 10^{-12} \text{ cm}^3 \text{ s}^{-1}$	g
$N_2 + e^- \rightarrow N_2^* + e^-$	$K_9 = 5.81 \times 10^{-9} \exp(-7.57/T_e) \text{ cm}^3 \text{ s}^{-1}$	h
$N_2^* \rightarrow N_2 + h\nu$	$\tau_{hv} = 2.3 \times 10^{-4} \text{ s}$	g
$N(\text{wall}) \rightarrow \frac{1}{2} N_2(g)$	$\tau_N^{-1} = D_N / \Lambda_N^2 \text{ s}^{-1}$	i
$Ar^+ + N_2 \rightarrow N_2^+ + Ar$	$K_{10} = 1.2 \times 10^{-11} \text{ cm}^3 \text{ s}^{-1}$	j
$Ar + e^- \rightarrow Ar^* + e^-$	$K_{11} = 2.2 \times 10^{-8} \exp(-12.4/T_e) \text{ cm}^3 \text{ s}^{-1}$	k
$Ar^* + e^- \rightarrow Ar^+ + 2e^-$	$K_{12} = 2.1 \times 10^{-7} \exp(-5.3/T_e) \text{ cm}^3 \text{ s}^{-1}$	l
$Ar + e^- \rightarrow Ar^+ + 2e^-$	$K_{13} = 1.23 \times 10^{-7} \exp(-18.68/T_e) \text{ cm}^3 \text{ s}^{-1}$	m
$Ti + e^- \rightarrow Ti^+ + 2e^-$	$K_{14} = 2.34 \times 10^{-7} \exp(-7.25/T_e) \text{ cm}^3 \text{ s}^{-1}$	n
$Ti + Ar^* \rightarrow Ti^+ + Ar + e^-$	$K_{15} = \sigma_{Ti} \cdot \nu_{th-Ti} \text{ cm}^3 \text{ s}^{-1}$	o

Tao – Ionized PVD of TiN – Comparison to Experiments

- Tao *et al.* tested their model using experimental measurements in the IPVD chamber.
- Decent model – experiment agreement achieved.
- Assumed different sticking coefficient for N at low and high N₂ flows to explain experimental observation.

TiN IPVD Model – Experiment Comparison

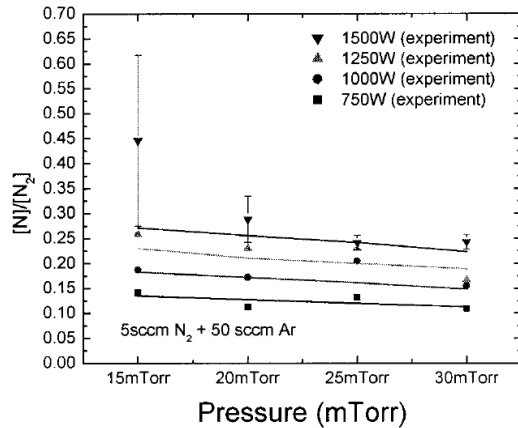


FIG. 3. Comparison of the experimental dissociation of nitrogen (symbols) and the computed dissociation (solid lines).

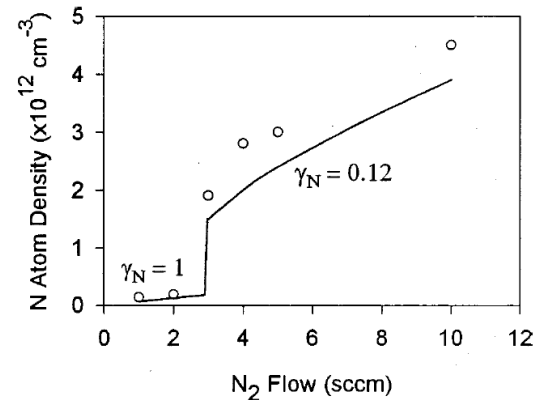


FIG. 4. The modeled atomic nitrogen density (solid line) is compared with experimental measurements (O) described in Ref. 11. The increase in [N] at 3 sccm is due to the experimentally observed transition from the metal target mode to the nitride target mode. The transition is modeled by decreasing the N wall loss parameter from $\gamma_N = 1$ to $\gamma_N = 0.12$. Plasma conditions were 15 mTorr total pressure, 1 kW plasma power, and 1 kW target power.

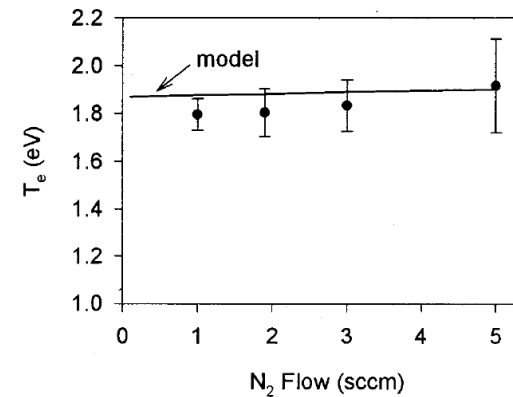


FIG. 5. Comparison of computed and measured electron temperature.

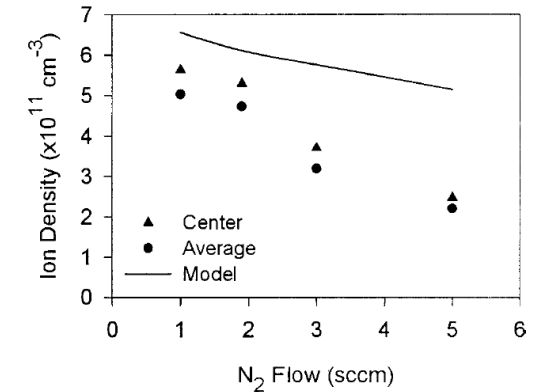
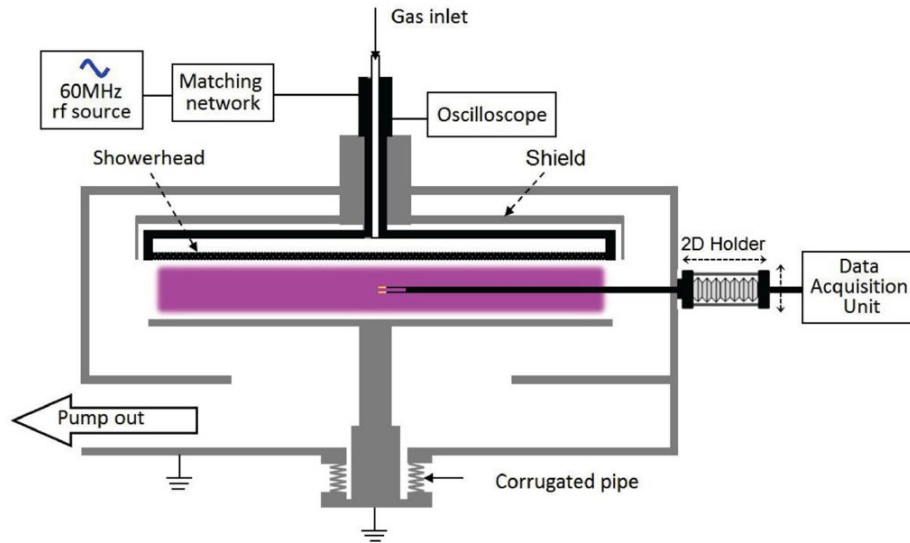


FIG. 6. Comparison of the computed global ion density with the ion density measured at the center of the discharge and the average ion density.

Liang – 60 MHz N₂ Capacitively Coupled Plasma – Model

- Liang *et al.* developed a 2D fluid model of N₂ capacitively coupled plasma (CCP) operating at 60 MHz.
- The model was tested against experimentally measured N₂⁺ ion density.
- Model was used to understand the effect of RF power and inter-electrode gap on plasma uniformity.

60 MHZ CCP



N₂ Plasma Chemistry

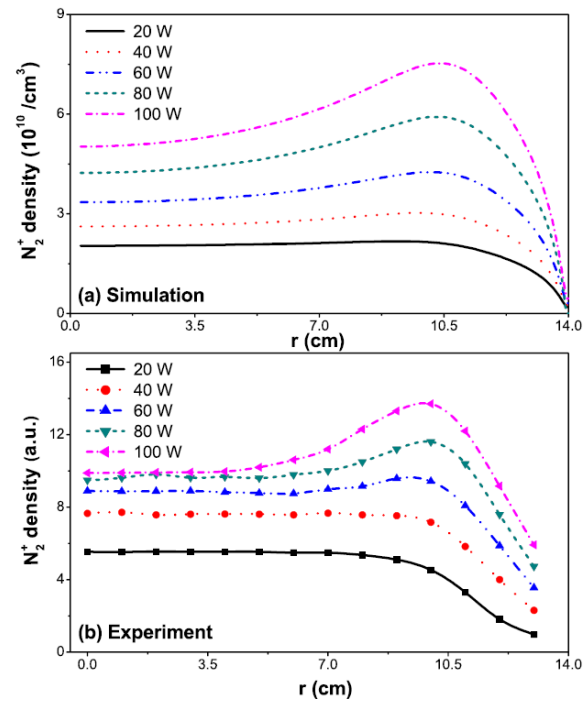
TABLE I. The reactions taken into account in the model.

No.	Reactions	Rate Coefficient ^a	ϵ^b	Reference
R1	$N_2 + e \rightarrow N_2 + e$	$1.04 \times 10^{-7} (T_e)^{0.43} \exp(-0.206/T_e)^c$		29
R2	$N + e \rightarrow N^+ + 2e$	$3.87 \times 10^{-9} (T_e)^{0.86} \exp(-14.62/T_e)^c$	14.54	29
R3	$N_2 + e \rightarrow N_2^+ + 2e$	$7.76 \times 10^{-9} (T_e)^{0.79} \exp(-16.75/T_e)^c$	15.60	29
R4	$N_2 + e \rightarrow N_2(A) + e$	$8.06 \times 10^{-10} (T_e)^{-0.306} \exp(-8.87/T_e)^c$	6.17	29
R5	$N_2 + e \rightarrow N_2(B) + e$	$1.56 \times 10^{-8} (T_e)^{-0.52} \exp(-9.16/T_e)^c$	7.35	29
R6	$N_2 + e \rightarrow N_2(a') + e$	$6.6 \times 10^{-9} (T_e)^{-0.66} \exp(-11.05/T_e)^c$	8.40	29
R7	$N_2^+ + e \rightarrow N + N$	$1.8 \times 10^{-7} (T_e)^{-0.39c}$		15
R8	$N_2 + e \rightarrow N + N + e$	$2.15 \times 10^{-8} \exp(-14.39/T_e)^c$	9.75	30
R9	$N_2(A) + N_2(a') \rightarrow N_2^+ + N_2 + e$	3.2×10^{-12}		31
R10	$N_2(a') + N_2(a') \rightarrow N_2^+ + N_2 + e$	5.0×10^{-11}		32
R11	$N_2^+ + N \rightarrow N^+ + N_2$	$7.21 \times 10^{-13} \exp(T_{gas}/300.0)^d$		31
R12	$N_2(A) + N \rightarrow N_2 + N$	2.0×10^{-12}		31
R13	$N_2(A) + N_2 \rightarrow N_2 + N_2$	3.0×10^{-18}		33
R14	$N_2(A) + N_2(A) \rightarrow N_2(B) + N_2$	7.7×10^{-11}		16
R15	$N_2(B) + N_2 \rightarrow N_2(X_{v=0}) + N_2$	1.5×10^{-12}		34
R16	$N_2(B) + N_2 \rightarrow N_2(A) + N_2$	2.85×10^{-11}		34
R17	$N_2(a') + N_2 \rightarrow N_2(B) + N_2$	1.9×10^{-13}		16
R18	$N + N + N \rightarrow N_2(B) + N_2$	$8.27 \times 10^{-34} \exp(500.0/T_{gas})^{d,e}$		16
R19	$N + N + N_2 \rightarrow N_2 + N$	1.0×10^{-32e}		33
R20	$N_2(B) \rightarrow N_2(A) + h\nu$	2.0×10^{5f}		16

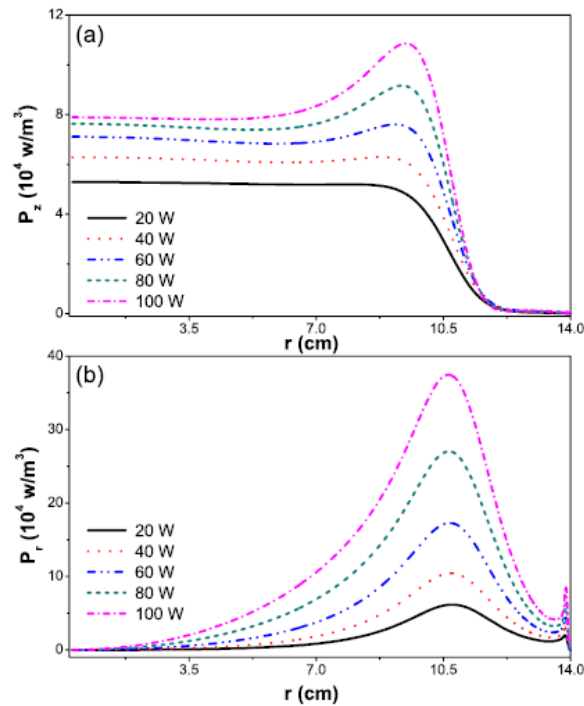
Liang – 60 MHz N₂ Capacitively Coupled Plasma – Plasma Uniformity

- The model showed that plasma intensified closer to the electrode edge as power increased.
- Plasma uniformity worsening with power linked to P_r at electrode edge increasing more rapidly than P_z .
- Demonstrated using model that inter-electrode gap can be increased to improve plasma uniformity.

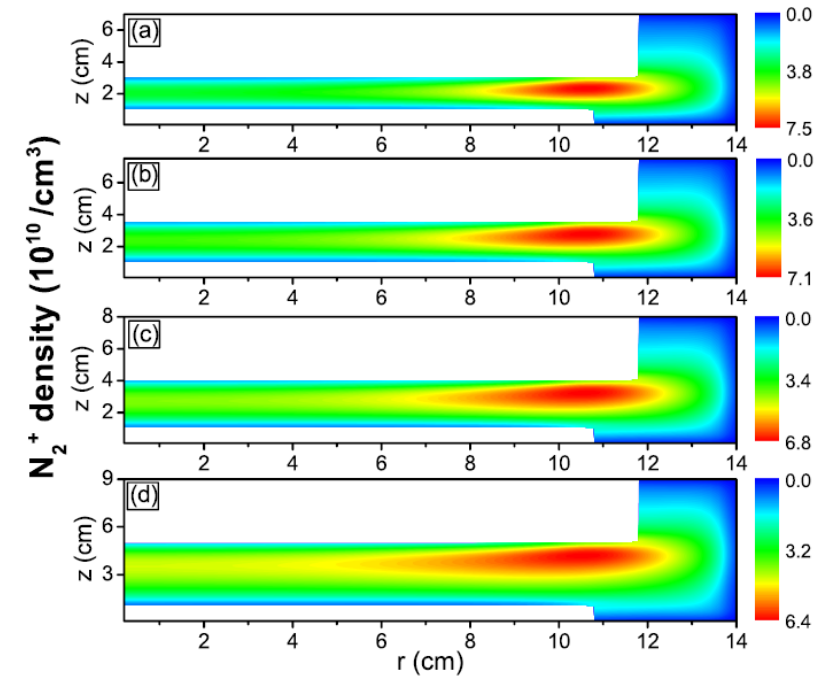
N₂⁺ Density



Power



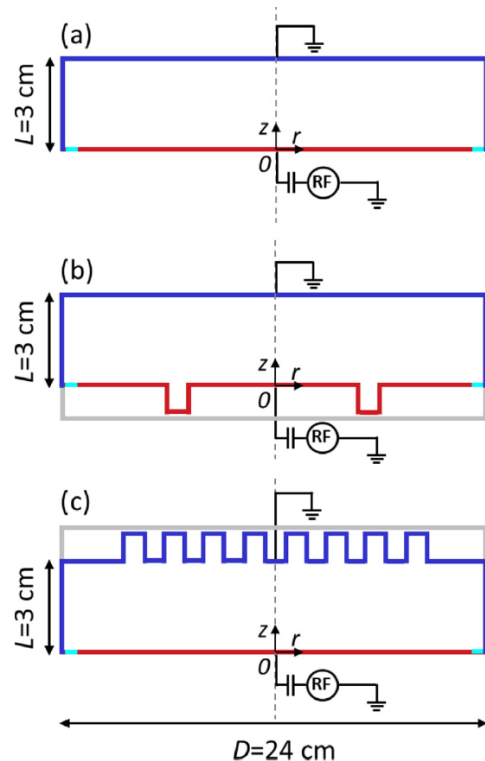
N₂⁺ Density vs. Gap



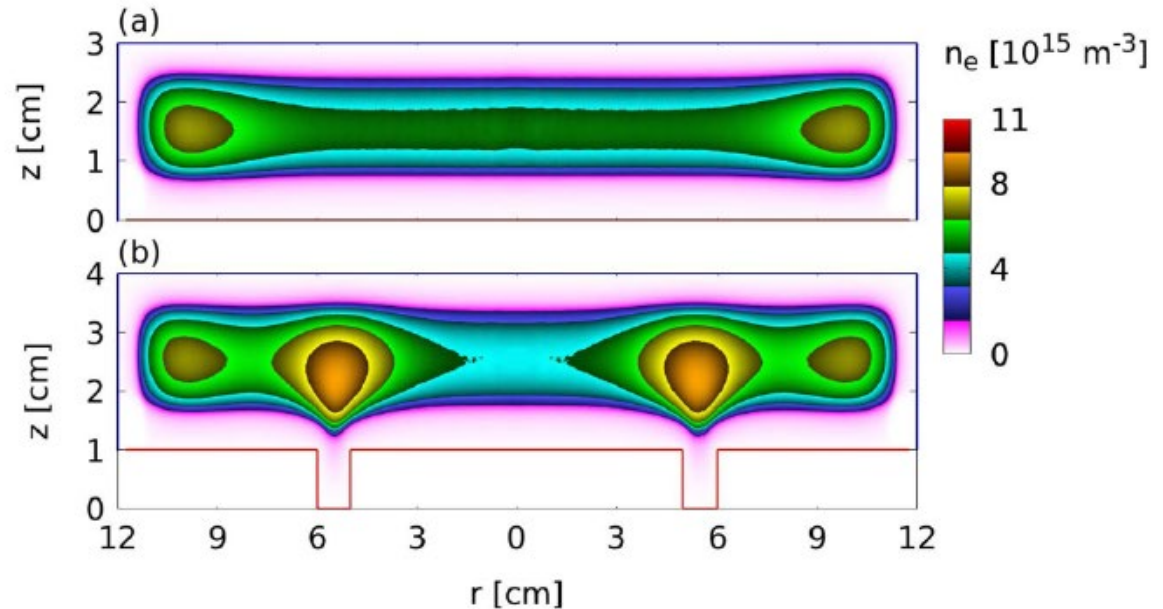
Wang – Uniformity Control in Capacitive Discharge – Model

- Wang *et al.* used a 2D PIC/MCC model to simulate a cylindrical 13.56 MHz CCP.
- Examined the effect of introducing trenches in the top (grounded) and bottom (powered) electrode.
- Simulations done for Ar plasma, 10 Pa, 1024 points in radial + axial directions, and > 7 million particles.

Chamber Geometry



Electron Density

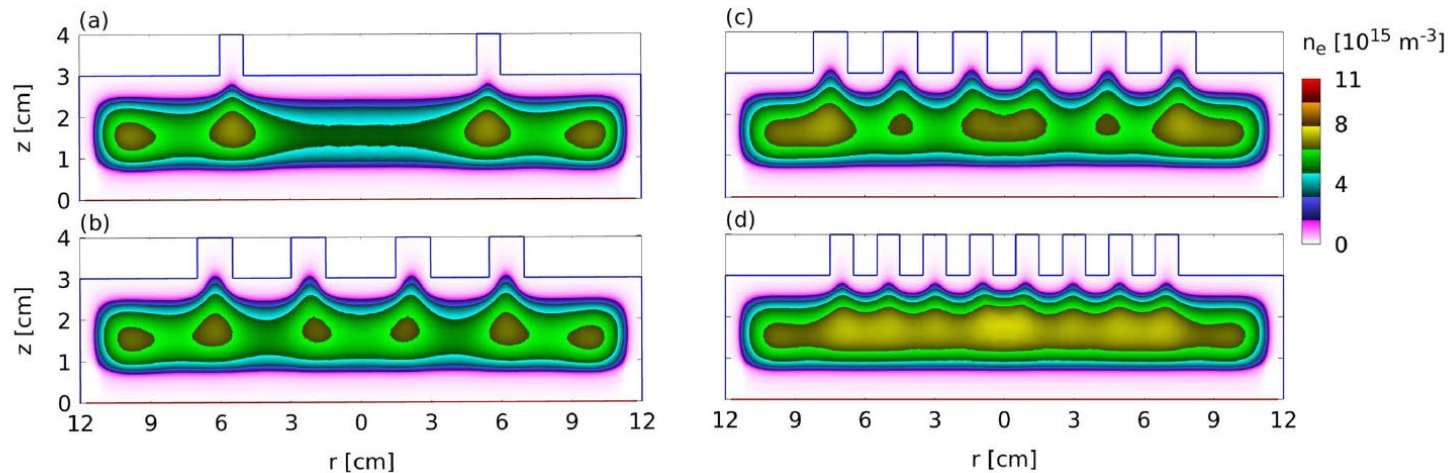


Wang *et al.*, J. Vac. Sci. Technol. A 39, 063004 (2021)

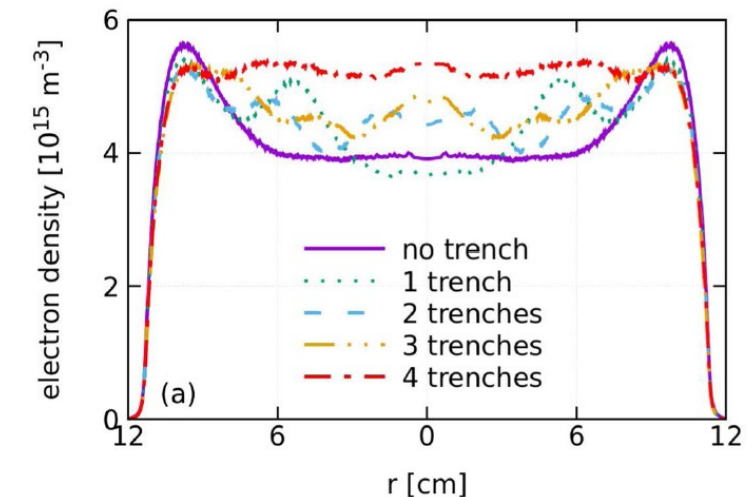
Wang – Uniformity Control in Capacitive Discharge – Testing New Concept

- The plasma density peaked at chamber edge due to strong electron heating at powered electrode edge.
- Found that electron heating enhances near trench corners, intensifying the plasma in the trench's vicinity.
- Demonstrated that multiple ring-shaped trenches can be used to improve the plasma uniformity.

Electron Density



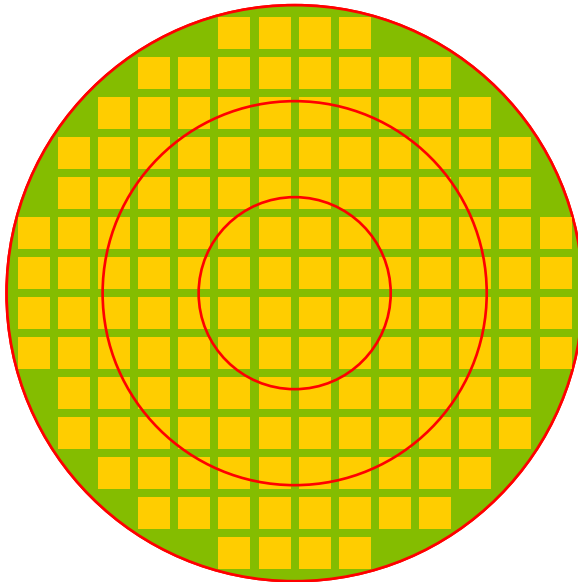
Electron Density vs. r



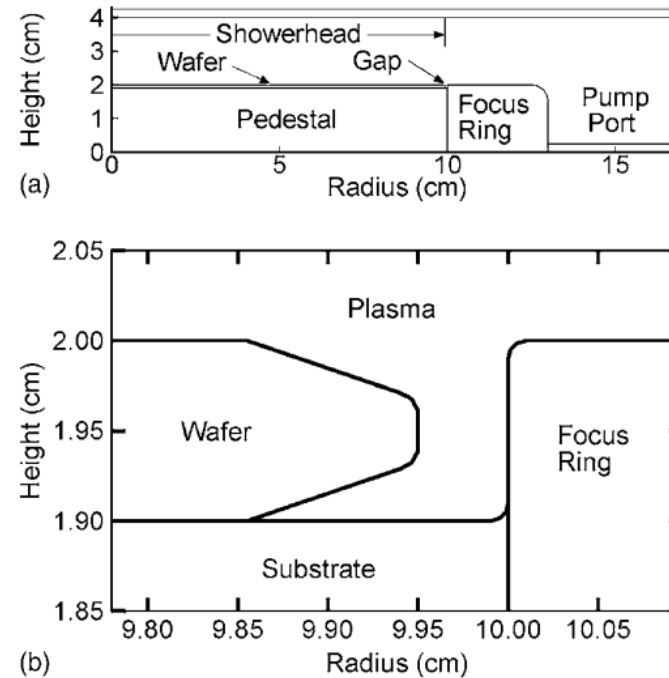
Babaeva – Plasma at Wafer Edge – Model

- Babaeva and Kushner examined the effect of the gap between wafer and focus ring.
- 2D simulations of the CCP discharge were done using nonPDPSIM, a fluid plasma model.
- Simulations were done for Ar/CF₄ plasma at 90 mTorr with 10 MHz power.

Dies on Wafer



Chamber Geometry



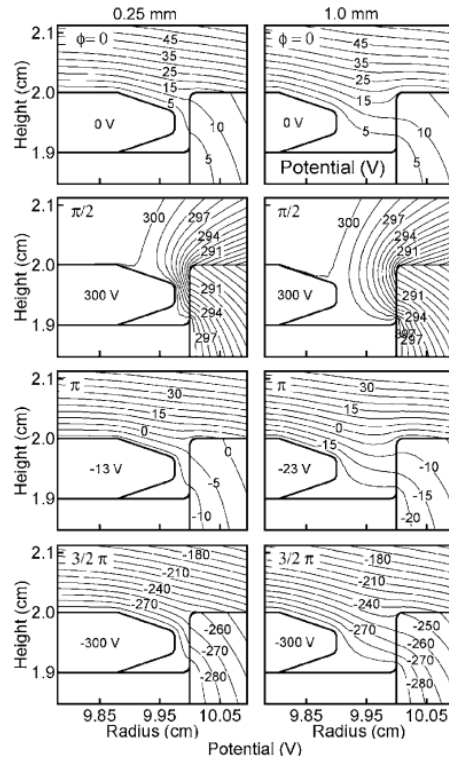
Ar/CF₄ Chemistry

	Species	
Ar	CF ₄	CF ₃ ⁺
Ar ^{+(4s)}	CF ₂	CF ₂ ⁺
Ar ^{+(4p)}	CF ₃	F ⁺
CF	CF	C ⁺
	F ₂	
	F	
Reactions ^a	Rate coefficient ^b	Reference
Electron Impact^c		
e + Ar → Ar ⁺ + e	c	10
e + Ar → Ar ⁺ + e	c	10
e + Ar → Ar ⁺⁺ + e + e	c	11
e + Ar → Ar ⁺⁺ + e + e	c	12
e + Ar ⁺ → Ar ⁺⁺ + e	c	10
e + Ar ⁺ → Ar ⁺⁺ + e	c	13
e + Ar ⁺ → Ar ⁺⁺ + e	c	10
e + CF ₄ → CF ₃ + F	c	15
e + Ar ⁺ → Ar ⁺⁺ + e	c	13
e + CF ₄ → CF ₃ + F	c	15
e + CF ₄ → CF ₃ + F	c	15
e + CF ₄ → CF ₃ + F + e	c	15 ^d
e + CF ₄ → CF ₃ + F + e	c	15
e + CF ₄ → CF ₃ + F + e	c	15
e + CF ₄ → CF ₃ + F + e	c	15
e + CF ₄ → CF ₃ + F + e	c	16 ^e
e + CF ₄ → CF ₃ + F + e	c	15 ^f
e + CF ₄ → CF ₃ + F + e	c	15 ^g
e + CF ₄ → CF ₃ + F + e	c	17
Neutral heavy particle reactions:		
Ar ⁺ + Ar ⁺ → Ar ⁺⁺ + Ar	1.0 × 10 ⁻⁹	18
Ar ⁺ + Ar ⁺ → Ar ⁺⁺ + Ar	1.0 × 10 ⁻⁹	18
Ar ⁺ + Ar ⁺ → Ar ⁺⁺ + Ar + e	1.0 × 10 ⁻⁹	18
Ar ⁺ - Ar ⁺	2.0 × 10 ⁻⁸	19
F + CF ₄ → CF ₃	2.0 × 10 ⁻¹¹	19
F + CF ₄ → CF ₃	1.8 × 10 ⁻¹¹	20
F + CF ₄ → CF ₃	9.3 × 10 ⁻¹¹	21
F ₂ + CF ₄ → CF ₃ + F	8.0 × 10 ⁻¹¹	22
F ₂ + CF ₄ → CF ₃ + F	1.0 × 10 ⁻¹⁰	27
Ar ⁺ + CF ₂ → CF ₃ + F + Ar	4.0 × 10 ⁻¹¹	23 ^h
Ar ⁺ + CF ₂ → CF ₃ + F + Ar	4.0 × 10 ⁻¹¹	23 ⁱ
Ar ⁺ + CF ₂ → CF ₃ + F + Ar	4.0 × 10 ⁻¹¹	24
Ion-neutral particle reactions:		
Ar ⁺ + Ar → Ar ⁺⁺ + Ar	4.6 × 10 ⁻¹⁰	25
CF ₃ ⁺ + CF ₄ → CF ₃ + CF ₃ ⁺	1.0 × 10 ⁻⁸	26
CF ₃ ⁺ + F → CF ₃ + F ⁺	5.0 × 10 ⁻¹⁰	25
F + CF ₃ → CF ₃ + F	4.0 × 10 ⁻¹⁰	27
F + CF ₃ → CF ₃ + e	3.0 × 10 ⁻¹⁰	27
F + CF ₃ → CF ₃ + e	2.0 × 10 ⁻¹⁰	27
F + F → F ₂ + e	1.0 × 10 ⁻¹⁰	27
Ar ⁺ + CF ₂ → CF ₃ + Ar + F	4.8 × 10 ⁻¹⁰	28
Ar ⁺ + CF ₂ → CF ₃ + Ar	7.0 × 10 ⁻¹⁰	28 ^k
Electro-ion and ion-ion reactions:		
e + Ar ⁺ → Ar	4.0 × 10 ⁻⁷ T _{pe,Ar} ^{0.5}	29
e + CF ₃ ⁺ → CF ₃ + F	3.0 × 10 ⁻⁷ T _{pe,CF3} ^{0.5}	27
CF ₃ ⁺ + CF ₃ ⁺ → CF ₃ + CF ₃	3.0 × 10 ⁻⁷	27
F + CF ₃ ⁺ → CF ₃ + F ⁺	8.7 × 10 ⁻¹⁰	25
F + CF ₃ ⁺ → CF ₃ + F + F	3.0 × 10 ⁻⁷ / (7300) ^{0.5}	27
F + CF ₃ ⁺ → CF ₃ + F	3.0 × 10 ⁻⁷	27
F + CF ₃ ⁺ → CF ₃ + F	3.0 × 10 ⁻⁷	30

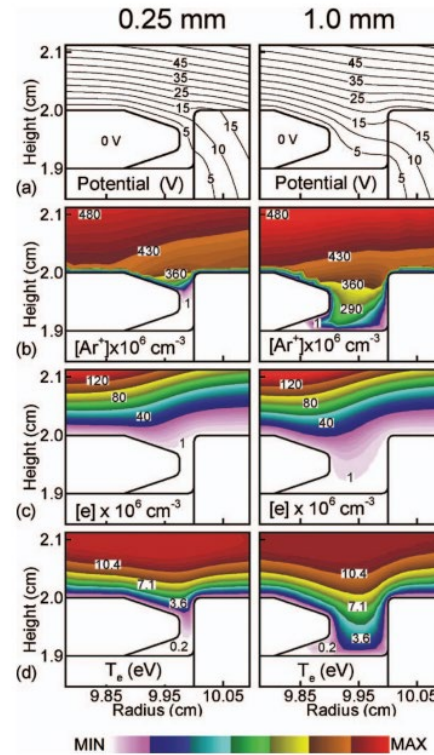
Babaeva – Plasma at Wafer Edge – Results

- As wafer edge – focus ring gap increased from 0.25 \rightarrow 1 mm, the plasma reached below the wafer edge.
- Demonstrated that height of focus ring can be used to control plasma penetration under the wafer edge.

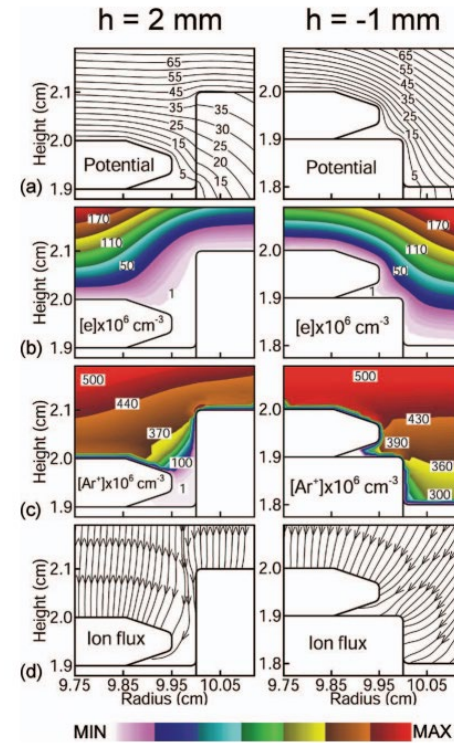
Potential vs. Time



Effect of Gap



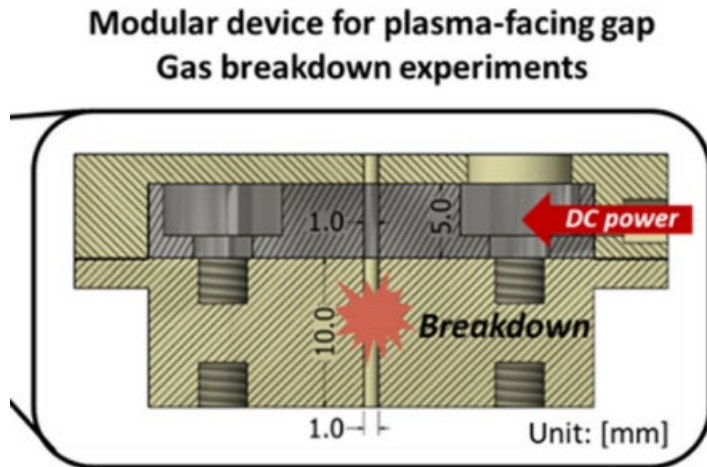
Effect of Ring Height



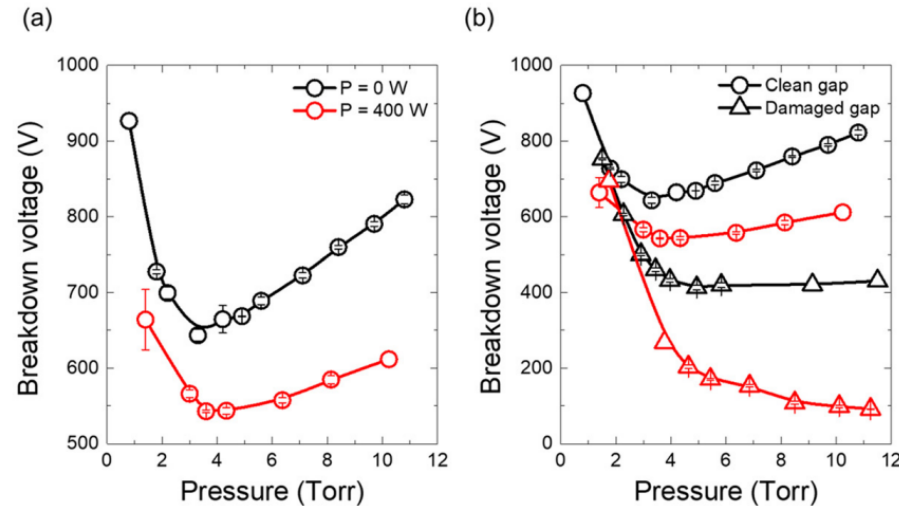
Son – Plasma Breakdown in Narrow Gap – Model

- Reliability is key for industrial products. Helping fix issues in an important part of engineers' job.
- This includes unintended gas breakdown in regions that should be plasma-free.
- Son *et al.* studied gas breakdown in narrow gaps which are exposed to the main plasma volume.
- EDIPIC was used to do 2D PIC/MCC simulations in Ar at 5 Torr. $\Delta x = 5 \mu\text{m}$, $\Delta t = 4 \text{ ps}$.

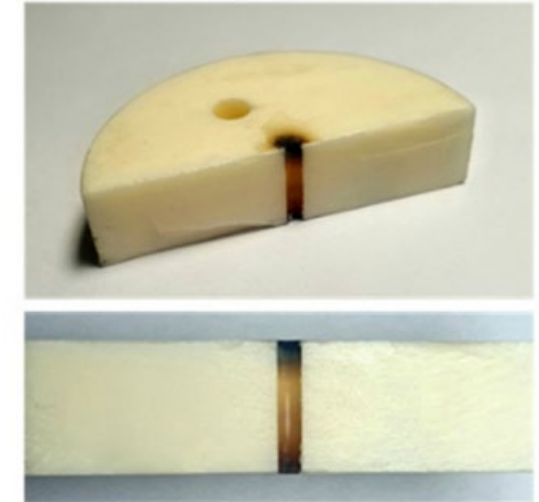
Geometry



Breakdown Voltage vs. Pressure



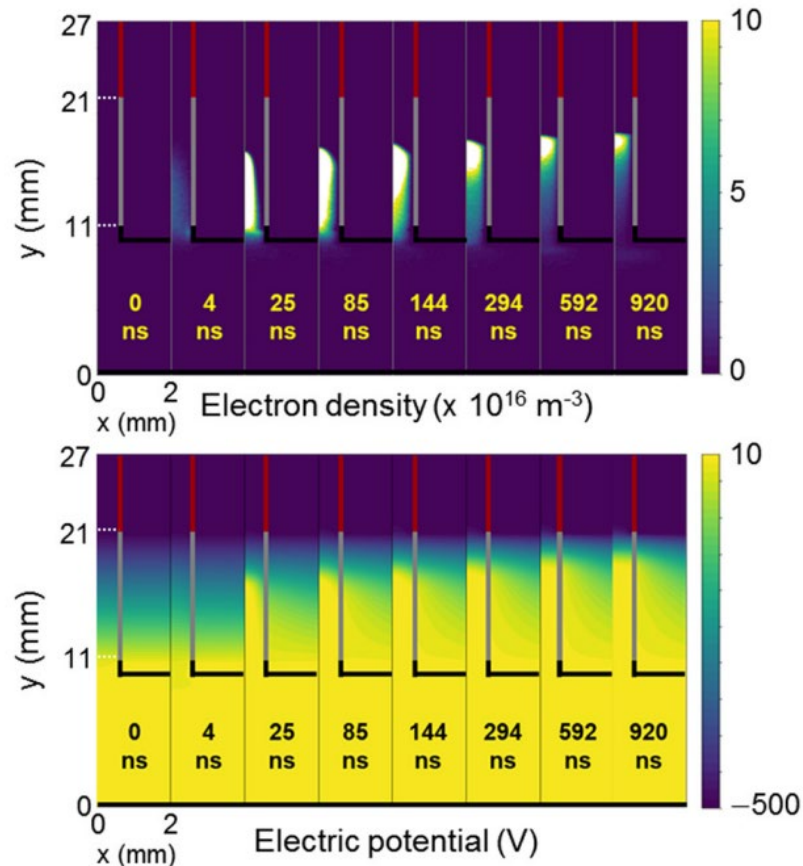
Damaged Material



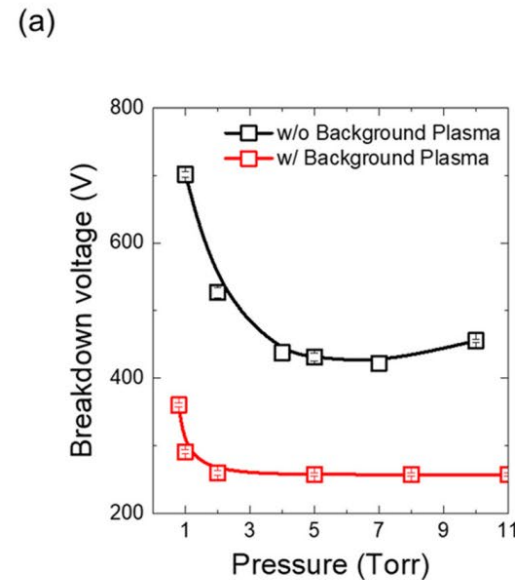
Son – Plasma Breakdown in Narrow Gap – Results

- They demonstrated that presence of low-density electrons in the gap significantly lowers the breakdown voltage.

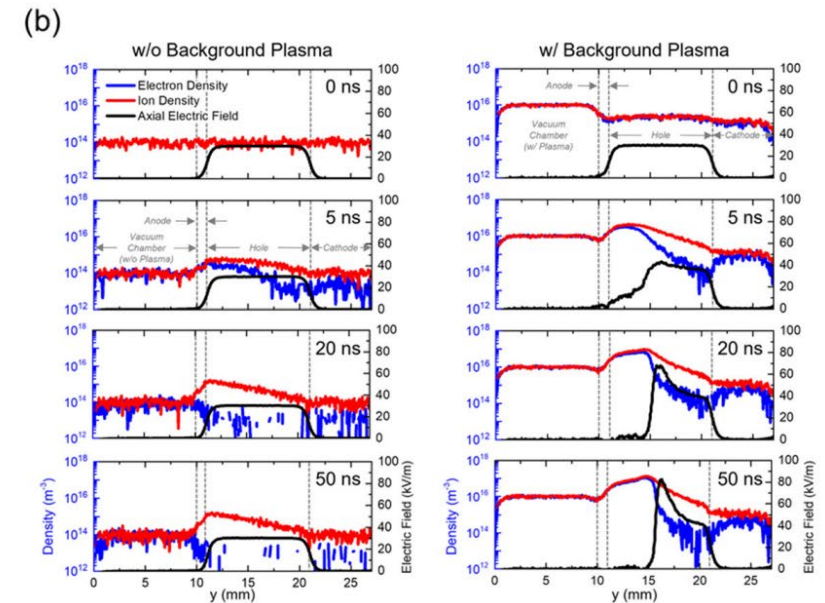
Plasma Ignition



Breakdown Voltage



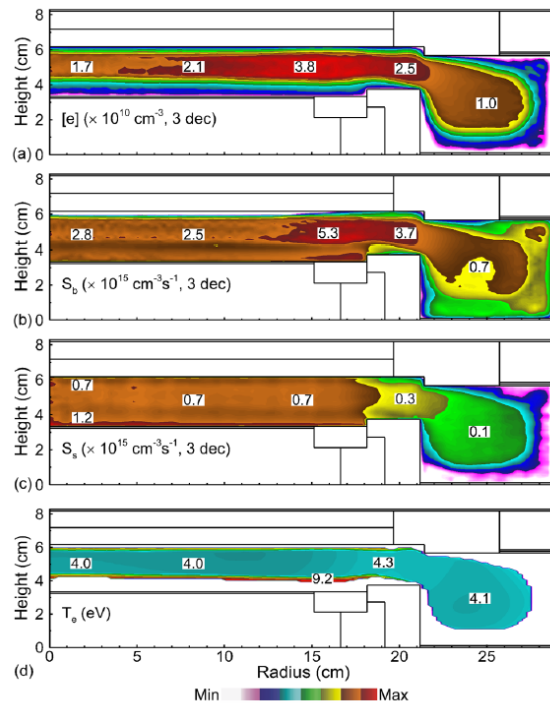
Density vs. Time



Huang – HAR Dielectric Etch – Model

- Huang *et al.* used a coupled plasma + feature scale model to examine high aspect ratio (HAR) dielectric etch.
- Plasma model: HPEM, feature scale model: MCFPM (University of Michigan).
- The model included detailed chemistry for Ar/C₄F₈/O₂ and a detailed mechanism for SiO₂ etch.

Plasma Properties



SiO₂ Etch Mechanism

TABLE I. Surface reaction mechanism for plasma etching of SiO₂ in Ar/C₄F₈/O₂ mixtures.

Gas phase species	Notes
ions, hot neutrals, and neutral particles	Ar ⁺ , Ar(h), Ar F ⁺ , F(h), F F ₂ ⁺ , F ₂ (h), F ₂ O ⁺ , O(h), O O ₂ ⁺ , O ₂ (h), O ₂ C ₄ F ₈ ⁺ , C ₄ F ₈ (h), C ₄ F ₈ CO, CO ₂ , COF, COH
Etch products	SiF ₄ , SiF ₂
Spursted materials	R, SiO ₂ , Si
Surface sites	Notes
Photoactive	R(h)
Silicon oxide	SiO ₂ (s)
Pasivated oxide surface (complex)	SiO ₂ C ₄ F ₈ (s) SiOCF ₃ (s)
Silicon	Si(s)
Fluorinated silicon surface	SiF ₃ (s)
Polymer	P(s)
Activated surface sites	SiO ₂ C ₄ F ₈ ⁺ (s) SiOCF ₃ ⁺ (s) P ⁺ (s)
Reactions ^a	p ^b E _a (eV) ^c E _i (eV) ^d Notes
Activation of SiO ₂	
SiO ₂ (s) + I ⁺ → SiO ₂ ⁺ (s) + hν	0.9 70 140 1
Spurting of SiO ₂	
SiO ₂ (s) + I ⁺ → SiO ₂ + hν	0.9 70 140 1
Pasivation of SiO ₂	
SiO ₂ (s) + CF ₃ → SiO ₂ CF ₃ (s)	0.4 70 140 1
SiO ₂ (s) + CF ₂ → SiO ₂ CF ₂ (s)	0.3 70 140 1
SiO ₂ (s) + CF ₂ → SiO ₂ CF ₂ (s)	0.2 70 140 1
SiO ₂ (s) + C ₂ F ₄ → SiO ₂ C ₂ F ₄ (s)	0.2 70 140 1
SiO ₂ (s) + CF ₃ → SiO ₂ CF ₃ (s)	0.9 70 140 1
Further pasivation of complex	
SiO ₂ CF ₃ (s) + CF ₃ → SiO ₂ C ₂ F ₆ (s)	10 ⁻⁴ 70 140 1
SiO ₂ CF ₂ (s) + CF ₃ → SiO ₂ C ₂ F ₅ (s)	10 ⁻⁴ 70 140 1
SiO ₂ CF ₂ (s) + C ₂ F ₄ → SiO ₂ C ₂ F ₆ (s)	10 ⁻⁴ 70 140 1
SiO ₂ CF ₃ (s) + CF ₂ → SiO ₂ C ₂ F ₅ (s)	10 ⁻⁴ 70 140 1
SiO ₂ CF ₂ (s) + C ₂ F ₄ → SiO ₂ C ₂ F ₆ (s)	10 ⁻⁴ 70 140 1
SiO ₂ C ₂ F ₄ (s) + CF ₃ → SiO ₂ C ₂ F ₅ (s)	10 ⁻⁴ 70 140 1
Fluorination of pasivated surface	
SiO ₂ CF ₃ (s) + F → SiO ₂ CF ₂ (s)	0.1 70 140 1
SiO ₂ CF ₂ (s) + F → SiO ₂ CF ₂ (s)	0.1 70 140 1
SiO ₂ C ₂ F ₄ (s) + F → SiO ₂ C ₂ F ₃ (s)	0.1 70 140 1
Etching of pasivated surface complex	
SiO ₂ CF ₃ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ CF ₂ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₄ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₅ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₆ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₄ (s) + I ⁺ → SiO ₂ CF ₃ (s) + C ₂ F ₄ + hν	0.75 35 140 1

TABLE I. Continued

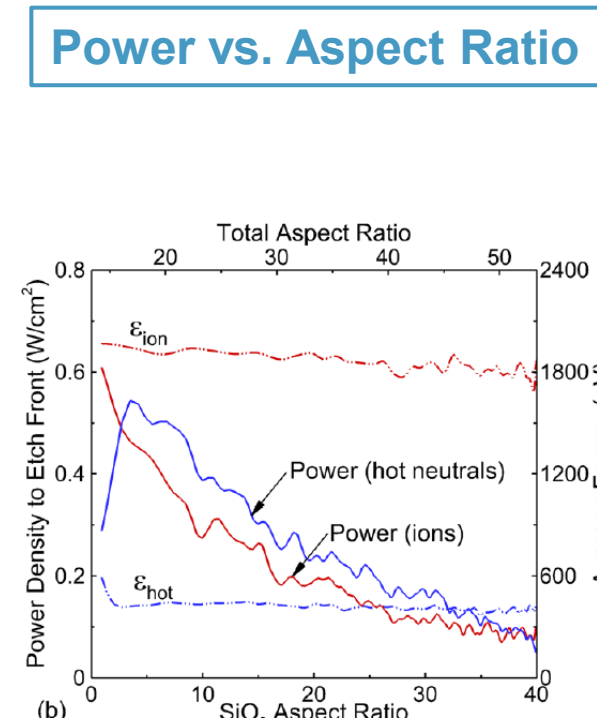
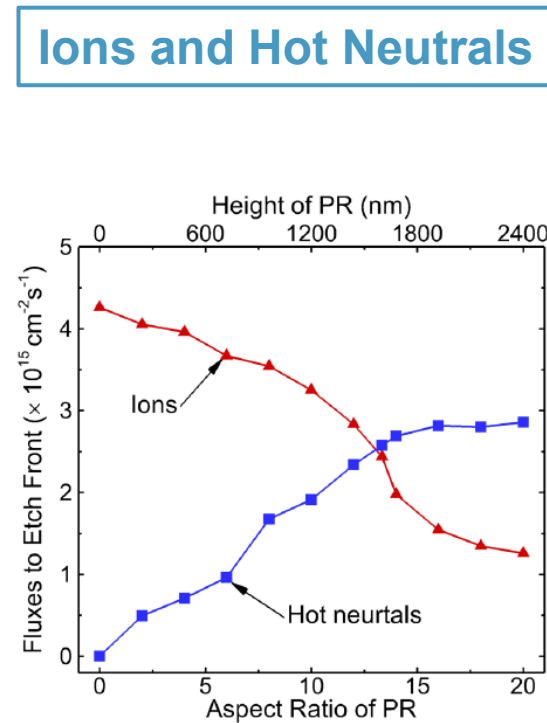
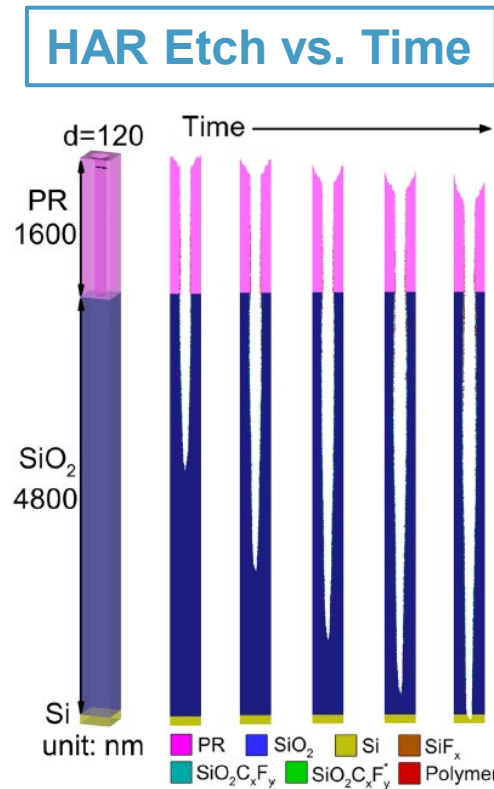
Reaction ^a	p ^b E _a (eV) ^c E _i (eV) ^d Notes
SiO ₂ C ₂ F ₄ (s) + I ⁺ → SiO ₂ CF ₃ (s) + C ₂ F ₄ + hν	0.75 35 140 1
SiO ₂ CF ₃ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ CF ₂ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₄ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₅ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₆ (s) + I ⁺ → SiF ₄ + CO ₂ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₄ (s) + I ⁺ → SiO ₂ CF ₃ (s) + C ₂ F ₄ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₅ (s) + I ⁺ → SiO ₂ CF ₂ (s) + C ₂ F ₄ + hν	0.75 35 140 1
SiO ₂ C ₂ F ₆ (s) + I ⁺ → SiO ₂ CF ₂ (s) + C ₂ F ₄ + hν	0.75 35 140 1
Polymer deposition on activated complex	
SiO ₂ C ₂ F ₄ (s) + CF ₃ → SiO ₂ C ₂ F ₅ (s) + P(s)	0.002 70 140 1
SiO ₂ C ₂ F ₅ (s) + CF ₃ → SiO ₂ C ₂ F ₆ (s) + P(s)	0.0015 70 140 1
SiO ₂ C ₂ F ₆ (s) + CF ₃ → SiO ₂ C ₂ F ₇ (s) + P(s)	0.001 70 140 1
SiO ₂ C ₂ F ₄ (s) + C ₂ F ₄ → SiO ₂ C ₂ F ₆ (s) + P(s)	0.001 70 140 1
SiO ₂ C ₂ F ₅ (s) + CF ₃ → SiO ₂ C ₂ F ₆ (s) + P(s)	0.002 70 140 1
SiO ₂ C ₂ F ₆ (s) + CF ₃ → SiO ₂ C ₂ F ₇ (s) + P(s)	0.0015 70 140 1
SiO ₂ C ₂ F ₇ (s) + CF ₃ → SiO ₂ C ₂ F ₈ (s) + P(s)	0.001 70 140 1
Polymer deposition on polymer	
P(s) + CF ₃ → P(s) + P(s)	0.002 70 140 1
P(s) + CF ₂ → P(s) + P(s)	0.0015 70 140 1
P(s) + CF ₂ → P(s) + P(s)	0.001 70 140 1
P(s) + C ₂ F ₄ → P(s) + P(s)	0.001 70 140 1
P(s) + O ₂ → P(s) + P(s)	0.02 70 140 1
P(s) + O ₂ → P(s) + P(s)	0.02 70 140 1
P(s) + O ₂ → P(s) + P(s)	0.02 70 140 1
P(s) + O ₂ → P(s) + P(s)	0.02 70 140 1
Polymer chemical sputtering	
P(s) + I ⁺ → hν + CF ₃	0.3 30 140 1
P(s) + I ⁺ → hν + CF ₂	0.3 30 140 1
P(s) + O ⁺ → COF	0.2 20 100 1
P(s) + O ₂ ⁺ → COF	0.2 20 100 1
P(s) + O ₂ ⁺ → COF	0.2 20 100 1
P(s) + O ₂ ⁺ → COF	0.2 20 100 1
Polymer chemical erosion	
P(s) + F → CF ₃	0.001 70 140 1
P(s) + F → CF ₂	0.001 70 140 1
P(s) + O → COF	0.5 70 140 1
P(s) + O → COF	0.9 70 140 1
Fluorination and etching of Si	
Si(s) + F → SiF ₃ (s)	0.01 70 140 1
SiF ₃ (s) + F → SiF ₄ (s)	0.02 70 140 1
SiF ₃ (s) + F → SiF ₄ (s)	0.03 70 140 1
SiF ₃ (s) + F → SiF ₄ (s)	0.05 70 140 1
Chemical, physical sputtering Si(s), SiF ₄ (s)	
Si(s) + I ⁺ → Si + hν	0.1 37.5 100 1
SiF ₄ (s) + I ⁺ → SiF ₄ + hν	0.3 10 100 1
SiF ₄ (s) + I ⁺ → SiF ₄ + hν	0.4 10 100 1
SiF ₄ (s) + I ⁺ → SiF ₄ + hν	0.5 10 100 1
Polymer deposition on Si(s) and SiF ₄ (s)	
Si(s) + CF ₃ → Si(s) + P(s)	0.5 70 140 1
Si(s) + CF ₂ → Si(s) + P(s)	0.375 70 140 1
Si(s) + CF ₂ → Si(s) + P(s)	0.25 70 140 1
Si(s) + C ₂ F ₄ → Si(s) + P(s)	0.25 70 140 1
SiF ₄ (s) + CF ₃ → SiF ₄ (s) + P(s)	0.002 70 140 1
SiF ₄ (s) + CF ₂ → SiF ₄ (s) + P(s)	0.0015 70 140 1
SiF ₄ (s) + CF ₂ → SiF ₄ (s) + P(s)	0.001 70 140 1
SiF ₄ (s) + C ₂ F ₄ → SiF ₄ (s) + P(s)	0.001 70 140 1

TABLE I. Continued

Reaction ^a	p ^b E _a (eV) ^c E _i (eV) ^d Notes
Redeposition of SiF ₄	
P(s) + SiF ₄ → P(s) + SiF ₄ (s)	0.001 70 140 1
Erosion of photoresist	
R(s) + I ⁺ → R + hν	0.01 10 ⁻⁵ 100 1
R(s) + O → COH	0.01 10 ⁻⁵ 100 1
Redeposition of gas phase photoresist	
W(s) + R → W(s) + R(s)	0.01 70 140 1
Polymer deposition on photoresist	
R(s) + CF ₃ → R(s) + P(s)	0.02 70 140 1
R(s) + CF ₂ → R(s) + P(s)	0.015 70 140 1
R(s) + CF ₂ → R(s) + P(s)	0.01 70 140 1
R(s) + C ₂ F ₄ → R(s) + P(s)	0.01 70 140 1
Activation by low energy ions	p ^b E _a (eV) ^c E _i (eV) ^d Notes
SiO ₂ C ₂ F ₄ (s) + I ⁺ → SiO ₂ C ₂ F ₅ (s) + hν	0.1 5 70 1
SiO ₂ CF ₃ (s) + I ⁺ → SiO ₂ CF ₂ (s) + hν	0.1 5 70 1
P(s) + I ⁺ → P(s) + hν	0.3 5 30 1
Polymer deposition by low energy ions	
SiO ₂ C ₂ F ₄ (s) + CF ₃ ⁺ → SiO ₂ C ₂ F ₅ (s) + P(s)	0.1 5 70 1
SiO ₂ C ₂ F ₅ (s) + CF ₃ ⁺ → SiO ₂ C ₂ F ₆ (s) + P(s)	0.1 5 70 1
SiO ₂ CF ₃ (s) + CF ₃ ⁺ → SiO ₂ CF ₂ (s) + P(s)	0.1 5 70 1
SiO ₂ CF ₂ (s) + CF ₃ ⁺ → SiO ₂ CF ₂ (s) + P(s)	0.1 5 70 1

Huang – HAR Dielectric Etch – Feature Scale Results

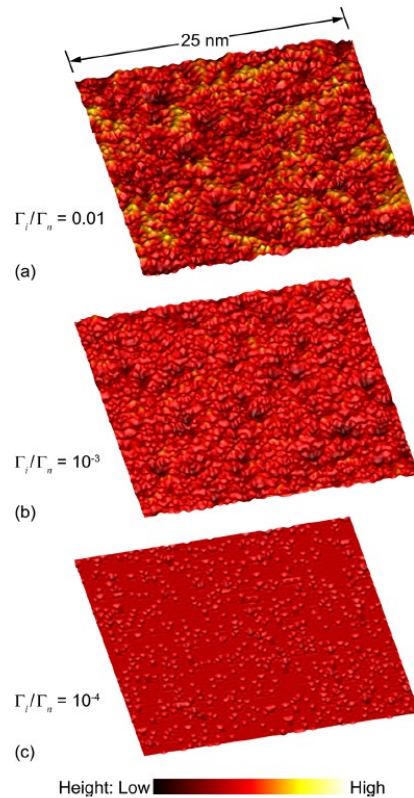
- Simulations were used to understand how the etch process evolves with increasing aspect ratio (AR).
- Ions converted to “hot neutrals” when they impacted the sidewalls inside trenches.
- Power delivered to the feature bottom decreased with AR due to increased energy loss on sidewall impact.
- They demonstrated how the profile can be controlled by changing the ratio of C_xF_y neutrals to ions.



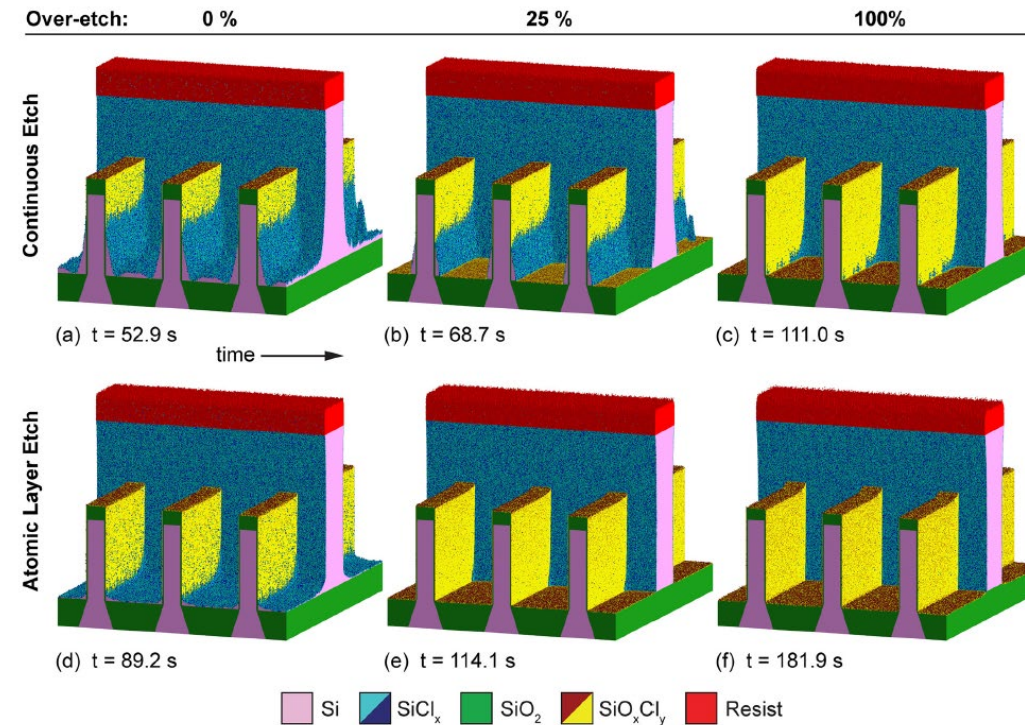
Huard – Si Atomic Layer Etch (ALE) – Feature Scale Results

- Huard *et al.* used the same codes (HPEM+MCFPM) to investigate Si ALE under non-ideal conditions.
- They found that high neutral / ion flux ratio is needed to get smooth surface during ALE.
- ALE during over-etching helps get clean fin profiles in less time with reduced damage.

Surface Roughness vs. Γ_i/Γ_n



Profile During Etch



Huard *et al.*, J. Vac. Sci. Technol. A 35, 031306 (2017).

Kuboi – PECVD Feature Scale Model

- Kuboi *et al.* studied plasma enhanced CVD deposition of Si_3N_4 in $\text{SiH}_4/\text{NH}_3/\text{N}_2$ and $\text{SiH}_4/\text{N}_2\text{O}$.
- Experiments showed that, when deposited at 120°C , the film is columnar at low flow rate.
- Modeling was done using a Monte Carlo feature scale model that included surface migration.

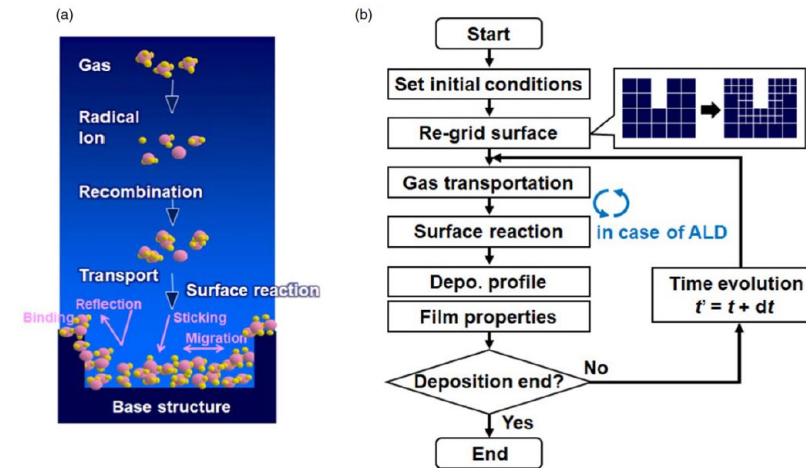
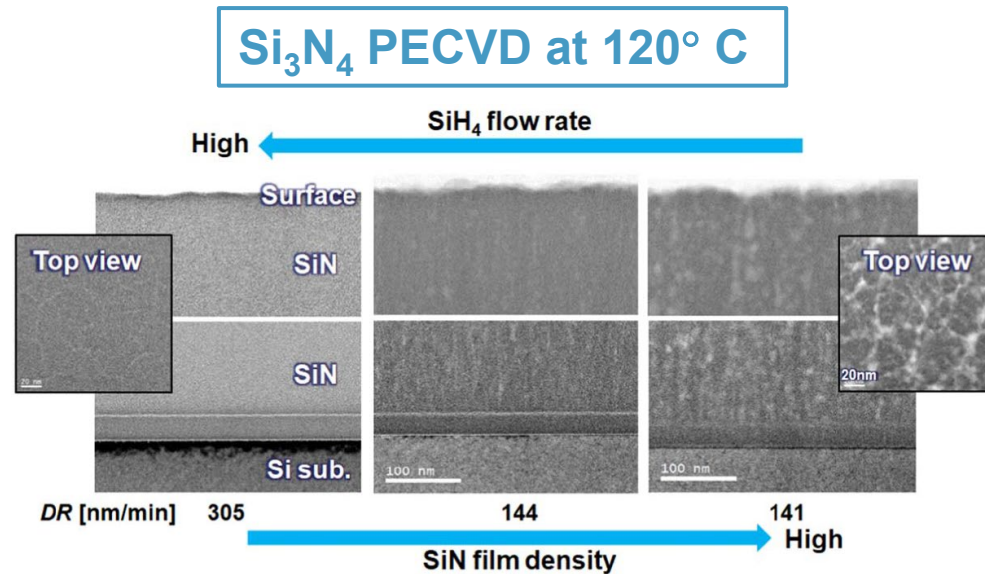


Fig. 2. (Color online) (a) Schematic of the deposition process and (b) calculation flow chart of the 3D deposition model.

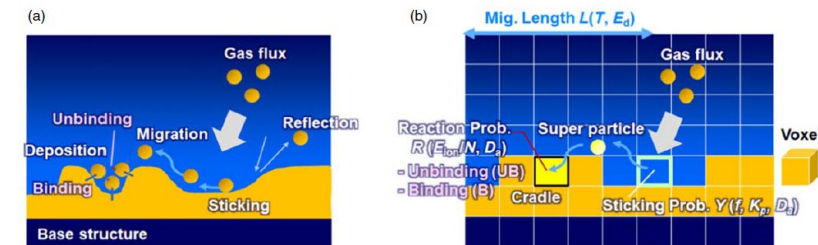
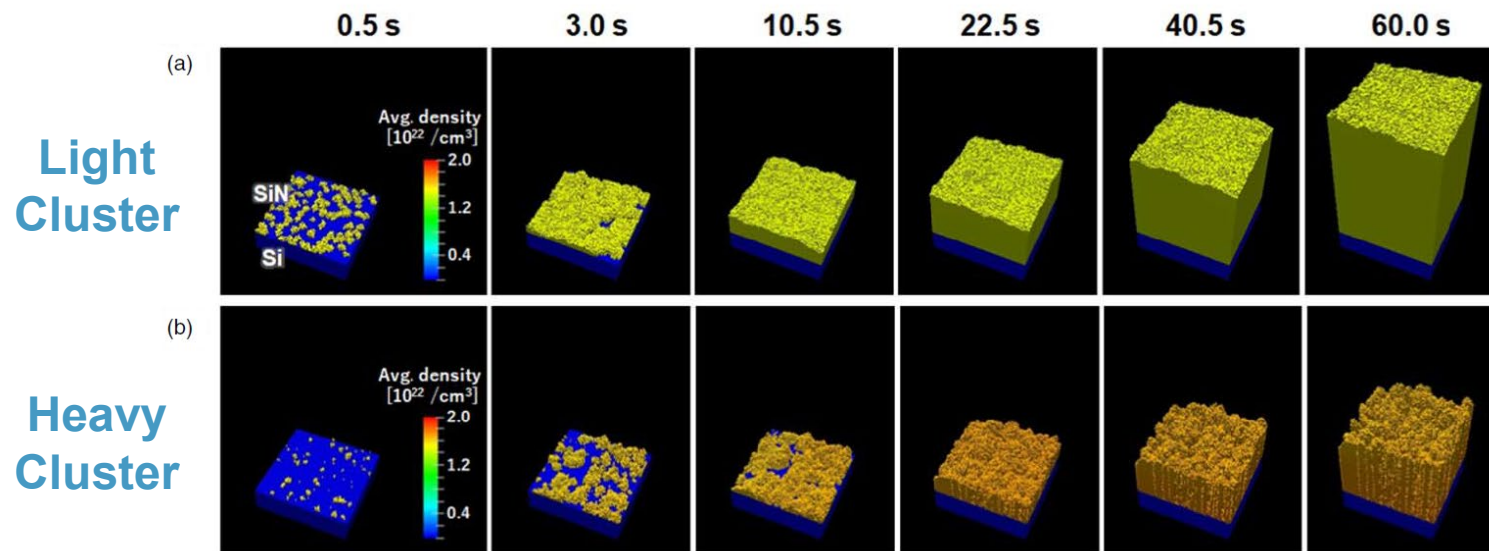


Fig. 3. (Color online) Schematic pictures of (a) actual phenomena on the deposited surface over the base structure: irradiation of gas, sticking, reflection, migration, and binding and (b) corresponding deposition model using a statistical ensemble method in the voxel space.

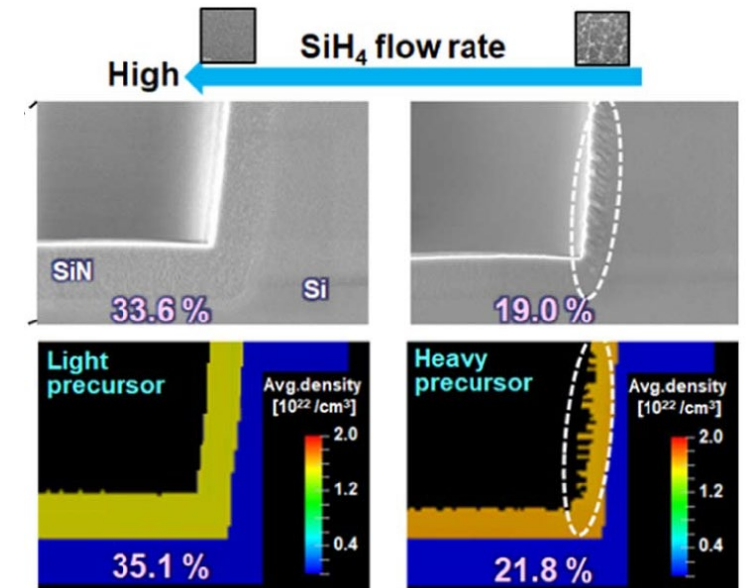
Kuboi – PECVD Feature Scale Model

- The structure of the film vs. SiH_4 flow was attributed to recombination in gas phase.
- Longer residence time at lower SiH_4 flow led to formation of larger clusters in the gas, producing columnar film growth.

Evolution of Deposited Film



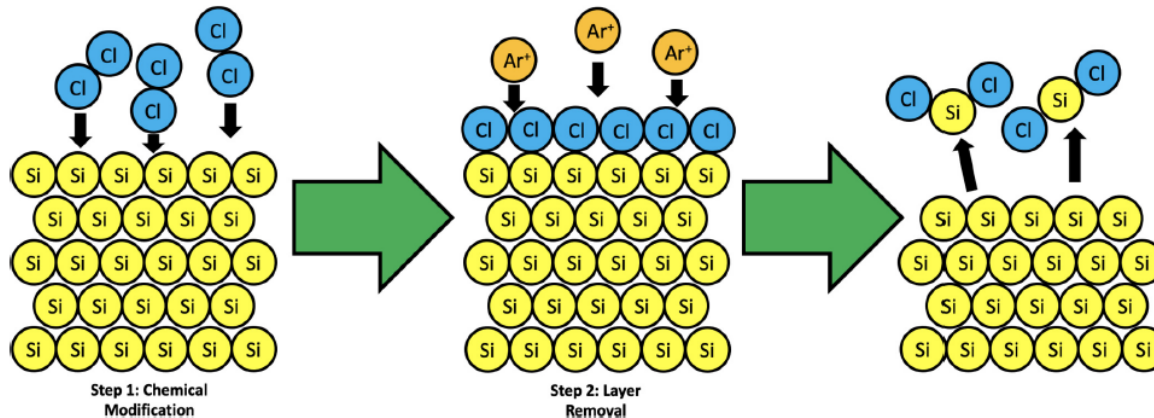
Film in Feature



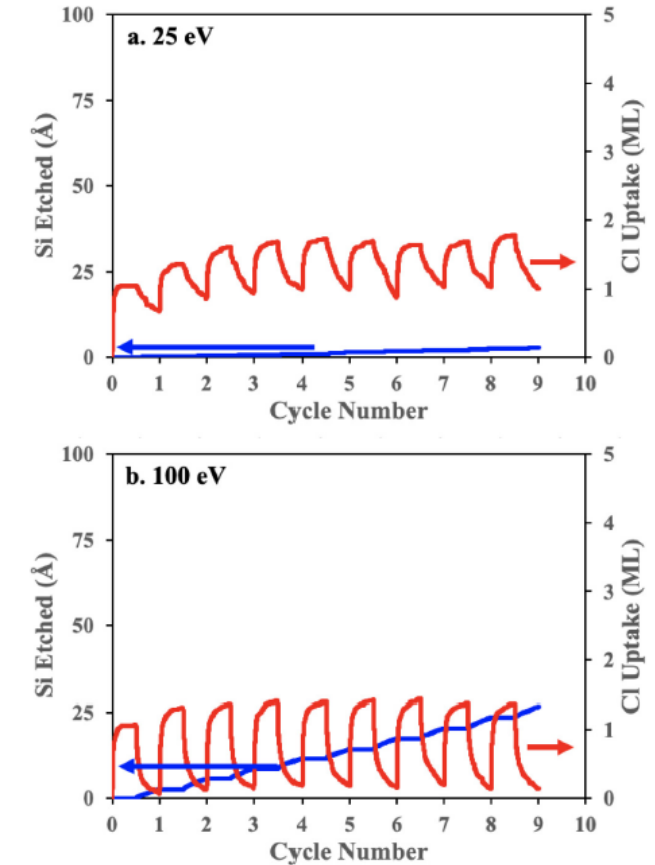
Vella – Si Atomic Layer Etch (ALE) – Molecular Dynamics (MD) Model

- Vella and Graves used a MD model to examine Si ALE in $\text{Cl}_2 + \text{Ar}$ plasma.
- They used the REBO potential developed earlier in their group to model the Si-Cl system.
- Etch is self-limiting and close to ideal ALE at 25 eV. The etch rate is low.
- With increasing ion energy, etching does not stop during the etch step.

Ideal Si- Cl_2 -Ar Atomic Layer Etch Process



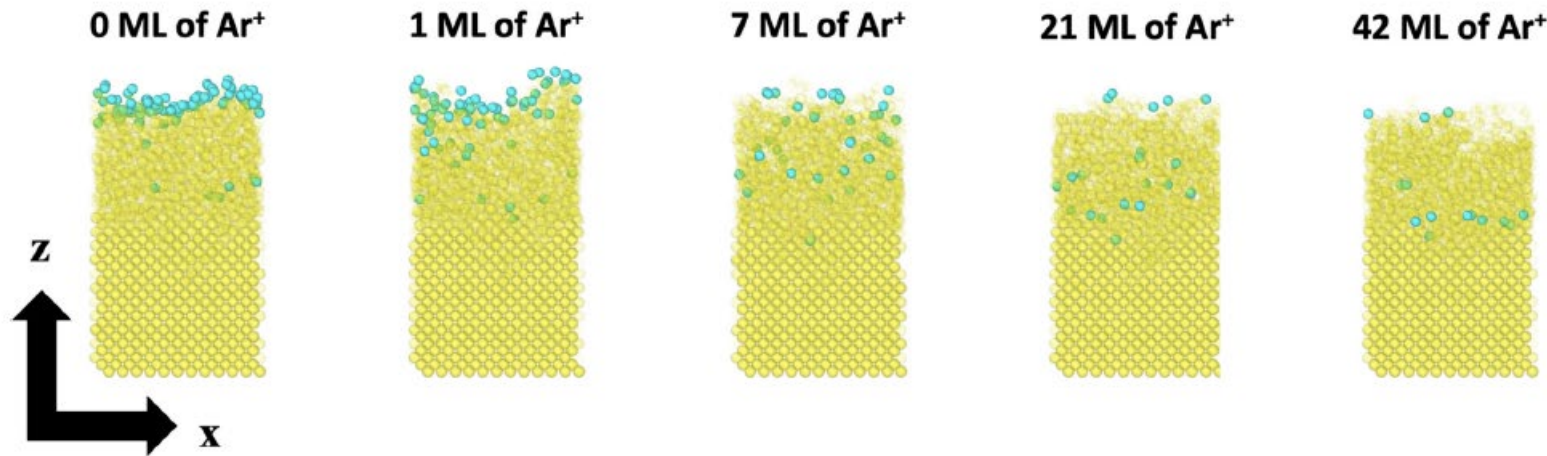
Si Etched vs. Time



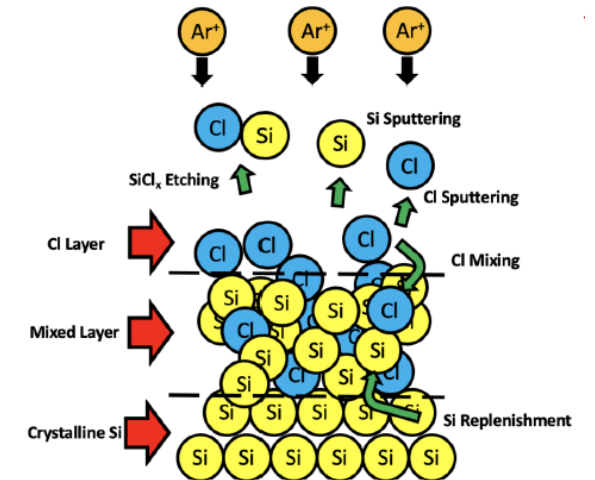
Vella – Si ALE – MD Results

- It was shown that if multiple ions are used during the ion bombardment step, the structure seen by the ion changes with time. The last ions experience a more physical sputtering like condition.
- Ions create a mixed layer near the surface with some residual Cl.

Si Structure After Ar^+ Bombardment



What's Happening Near the Surface?

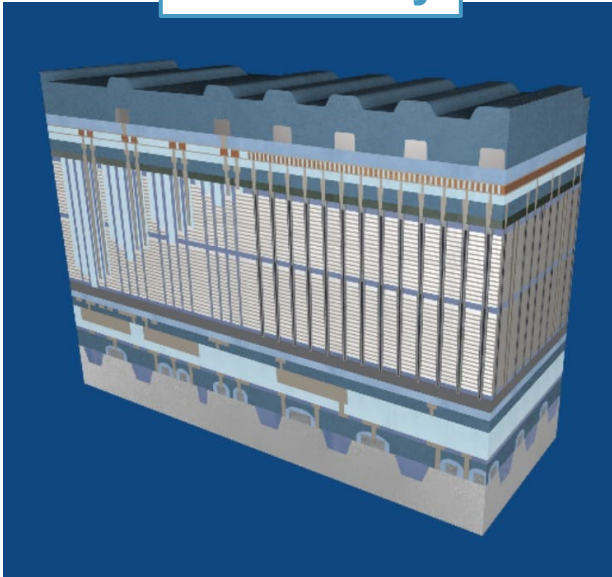


Conclusions

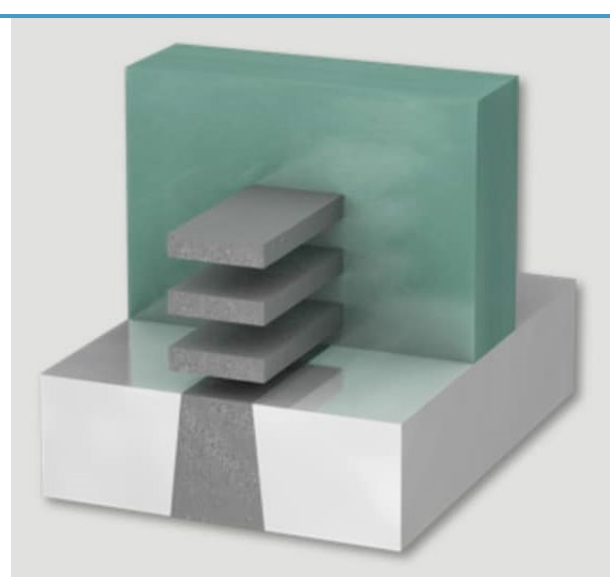
The Future of Plasma and Feature Scale Modeling

- Complexity of microelectronics technologies increasing immensely:
 - ▶ 3D architectures
 - ▶ nm-sized features
 - ▶ Atomic level precision during manufacturing on 300 mm wafers
- Precise control of every aspect of the plasma required.
- Resulting complexity making modeling ever more critical for advancing plasma technology.

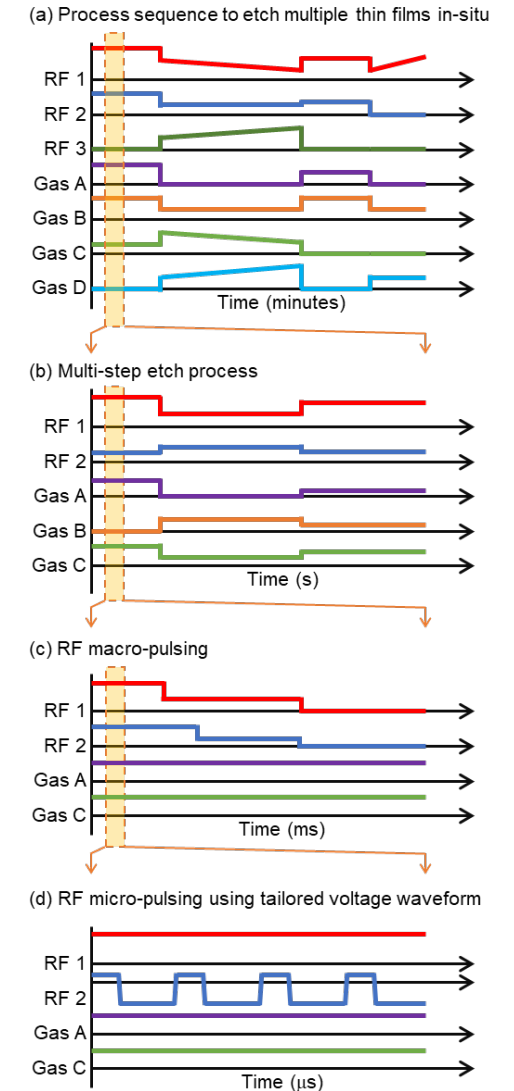
3D Memory



Gate All Around Transistor



Typical Plasma Etch Process



Conclusions

- Low T_e plasmas are a vital technology used for microelectronics manufacturing.
- Plasma modeling plays active role in plasma technology development in industry.
- Semiconductor industry is one of the largest employer of plasma modeling engineers.
- Plasma modeling engineers in industry:
 - ▶ Actively participate in R&D, product design, and customer communication
 - ▶ Use a variety of specialized software tools
 - ▶ Work on a diverse set of technically challenging problems
 - ▶ Need strong foundation in plasma physics and plasma – surface interactions to be successful
- Examples were used to illustrate the types of modeling work done in industry.
- Close connection to experiments and focus on solving major technological problems are key.

